Technical Document LA19036





Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

NRCB USE ONL	γ	 Application number	Legal land description
Approval		1019036	NF. 10-9-27 W94
Amendment			190

APPLICATION DIS LOSURE

This information is collected under the authority of the *Agricultural Operation Practices Act* (AOPA), and is subject to the provisions of the *Freedom of Information and Protection of Privacy Act*. This information is public unless the NRCB grants a written request that certain sections remain private.

Any construction prior to obtaining an NRCB permit is a offence and is subject to enforcement action, including prosecution.

I, the applicant, or applicant's agent, have read and understand the statements above, and I acknowledge that the information provided in this application is true to the best of my knowledge.

Date of sig

min ul wit

Corporate name (if applica, le)

GENERAL INFORMATION RE UIREMENTS

Proposed facilities. List all proposed confined feeding operation facilities and their measurements, including if it is an addition to a an existing facility (attach additional pages if needed)

Proposed manure collection areas & manure storage facilities	Dimensions (m)
Carer & Julter AO: Under Cover Pens	82 m x 15 m
3 comple 2 existing * I new AO: Open Pens AO: Size updated on Nov 17, 2020 to 36m x	$\frac{92 \text{ m x } 37 \text{ m}}{1 \text{ m x } 37 \text{ m}}$
Catch bash AO: Size updated on Nov 17, 2020 to 36m x 21m x 1.8m deep at applicants request	36m x 21m x 1.8m deep E5 M x 17M X 15 M
AO: The under cover and open pens are proposed to have roller	
compacted concrete liners. The catch basin is proposed to have	
a synthetic liner. The under cover and open pens have already	
been constructed.	

Existing facilities. List ALL existing confined feeding operation facilities and their measurements (use additional pages if needed)

Existing barns, manure collection areas & manure storage facility			Dimensions (m)	NRCB USE ONLY	
Barn 1		AO: East Hog Ba	arn	JUM X 12m	Confirmed
Barn 2	-	AO: West Hog Ba	arn .	60 mx 12m	Confirmed
Laguan	14	AO: East EMS	40 x 25 x 1.75 m deep	40 Mx 3 Mx 12	Confirmed
Lagain	45	AO: West EMS	20 x 20 x 2.5 m deep	291X 20 MX 2.5	Confirmed
The applic	cant red	quested on Nov 17,	2020 to add to their appli	cation to	
Decommission the concrete manure pit between the east hog barn and east EMS					
The applie	cation o		at the calf hutches north of		o be

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If a new facility is replacing an old facility, what will be done with the old facility and when? \Box N/A

Proposed construction completion date:

November 30, 2022

Additional information:

AO: A drilling report was provided on November 5, 2020 showing test hole locations and test hole soil logs. An engineering report prepared by Wood Environment and Infrastructure Solutions (Wood) was provided on October 29, 2020 and updated on November 6, 2020.

Photos showing the construction of the roller compacted concrete (RCC) pads (circa November 15, 2019) were provided on November 6, 2020

The report and photographs has been appended to the end of the TD.

This information was provided by the applicant to support their application following requests for information, in May, 2020, to show how the proposed alternative liner (constructed using RCC) can meet AOPA groundwater protection requirements.

Livestock Numbers: (include all livestock)

Note: Livestock numbers in this table will be used when processing the application)

Livestock type/ category	Existing number	Change in number (if applicable)	Total
Feeder Calves	0	+ 3000	3000
Feeder Calves Hugt Farrow to Wean	ડસ	-250	0
AO: The grandfathered hog barns are cu	, ,		
equipment and supplies. There are no h	0		
was carried out as part of this decision a summary. The determination identified t			
finish, or 171 sows farrow to wean.	liat the deethed capa	City as 04 SOWS 14110	N LO
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AO: Email from applicant requesting to add/change items on their application

From:	Arie and Willemiek Muilwijk
To:	Andy Cumming
Subject:	Permit Update
Date:	Tuesday, November 17, 2020 1:49:28 PM

Hello Andy,

Hope things are going well with you.

I would like to make some minor changes on the permit application.

- 1. Currently the catch basin size is listed at 31m long, 21m wide, and 1.8m deep. Could we change that to 36m long?
 - a. This would help with manure management
- 2. Could we add in the permit application that I would like to decommission a concrete lagoon that currently sits in between Barn 1 and Lagoon 1? Piping has already been diverted around this lagoon and it is not my intent to use it for manure storage any longer.

Thanks Arie

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AO: Barn 1 = East Barn
Lagoon 1 = East EMS
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AO: The concrete "lagoon" referred to is a deep concrete pit into which the manure from the East Barn flows , and from where the manure flows through a pipe into the East EMS.



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DECLARATION AND ACKNOWLEDGMENT OF APPLICANT CONCERNING WATER ACT LICENCE

issued by Alberta Environment and Parks (AEP) for a confined feeding operation (CFO)

Date and sign (or check) one of the following four options

OPTION 1: Applying through the NRCB for both the AOPA permit and the Water Act licence

I **DO** want my water licence application coupled to my AOPA permit application.

Signed this _____day of _____, 20____,

Signature of Applicant or Agent

OPTION 2: Processing the AOPA permit and Water Act licence separately

- 1. I (we) acknowledge that the CFO will need a new water licence from AEP under the *Water Act* for the development or activity proposed in this AOPA application.
- 2. I (we) request that the NRCB process the AOPA application **independently of** AEP's processing of the CFO's application for a water licence.
- 3. In making this request, I (we) recognize that, if this AOPA application is granted by the NRCB, the NRCB's decision will not be considered by AEP as improving or enhancing the CFO's eligibility for a water licence under the *Water Act*.
- 4. I (we) acknowledge that any construction or actions to populate the CFO with livestock pursuant to an AOPA permit in the absence of a Water Act licence will not be relevant to AEP's consideration of whether to grant the Water Act licence application.
- 5. I (we) acknowledge that any such construction or livestock populating will be at the CFO's sole risk if the *Water Act* licence application is denied or if the operation of the CFO is otherwise deemed to be in violation of the *Water Act*. This risk includes being required to de-populate the CFO and/or to cease further construction, or to remove "works" or "undertakings" (as defined in the *Water Act*).
- 6. CHECK IF RELEVANT I (we) acknowledge that the CFO is located in the South Saskatchewan River Basin and that, pursuant to the *Bow, Oldman and South Saskatchewan River Basin Water Allocation Order* [Alta. Reg. 171/2007], this basin is currently closed to new surface water allocations.
- Signed this _____ day of _____, 20_____,

OPTION 3: Additional water licence not required

1. I (we) declare that the CFO will not need a new licence from AEP under the *Water Act* for the development or activity proposed in this AOPA application.

Signed this _____ day of _____, 20_____

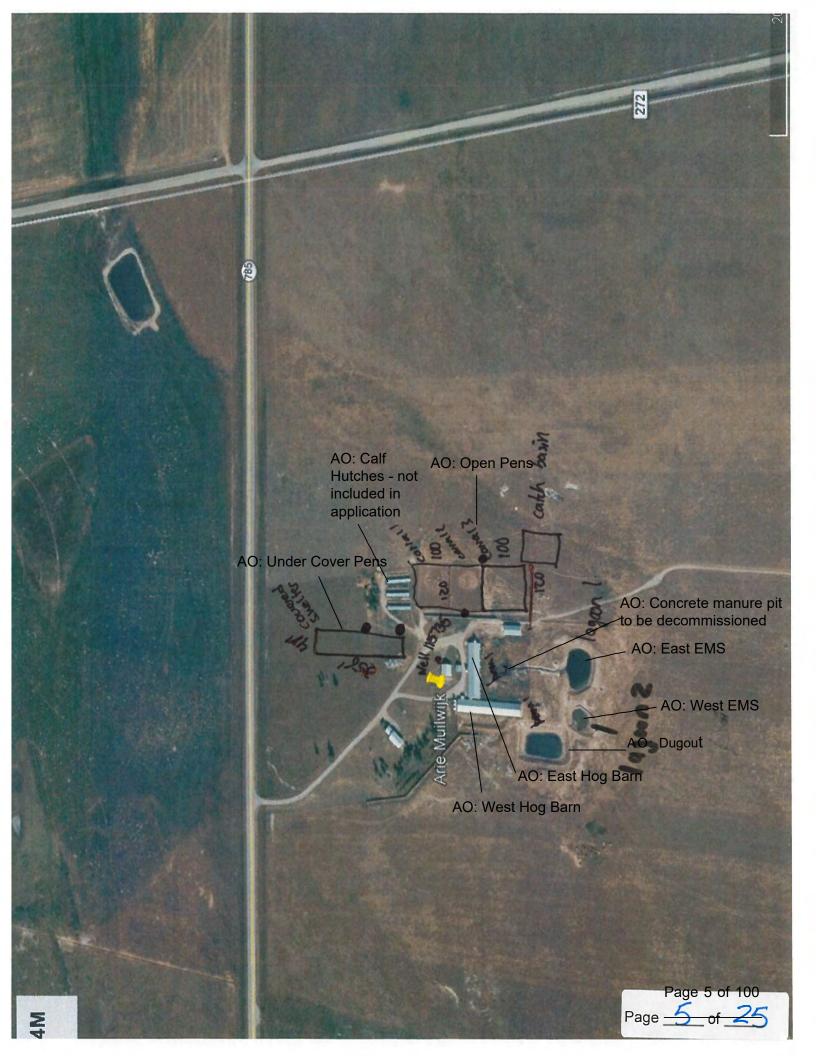
Signature of Applicant or Agent

Signature of Applicant or Agent

OPTION 4: Uncertain if Water Act licence is needed; acknowledgement of risk (for existing CFOs only)

- 1. At this time, I (we) do not know whether a new water licence is needed from AEP under the *Water Act* for the development or activity proposed in this AOPA application.
- 2. If a new *Water Act* licence is needed, I (we) request that the NRCB process the AOPA application **independently of** AEP's processing of the CFO's application for a water licence.
- 3. In making this request, I (we) recognize that, if this AOPA application is granted by the NRCB, the NRCB's decision will not be considered by AEP as improving or enhancing the CFO's eligibility for a water licence under the *Water Act*.
- 4. I (we) acknowledge that any construction or actions to populate the CFO with additional livestock pursuant to an AOPA permit in the absence of a *Water Act* licence will <u>not</u> be relevant to AEP's consideration of whether to grant my *Water Act* licence application, if a new water licence is needed.
- 5. I (we) acknowledge that any such construction or livestock increase will be at the CFO's sole risk if the *Water Act* licence application is denied or if the operation of the CFO is otherwise deemed to be in violation of the *Water Act*. This risk includes being required to de-populate the CFO and/or to cease further construction, or to remove "works" or "undertakings" (as defined in the *Water Act*).
- 6. CHECK IF RELEVANT I (we) acknowledge that the CFO is located in the South Saskatchewan River Basin and that, pursuant to the Bow, Oldman and South Saskatchewan River Basin Water Allocation Order [Alta. Reg. 171/2007], this basin is currently closed to new surface water allocations.

Signed this the hay of August, 2019.		In,	Signature	of Applicant or Agent
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GE	NERAL WATER INFORMATION - E	NRCB USE ONLY			
lico the evicting manife storage tacility that is closest to a			Comments	Meets regulations	
Wh ma	od plain information at is the elevation of the floor of the lowest nure storage or collection facility above the 5 year flood plain or the highest known flood el?	_ + (m)	Estimated From records	Not in known flood plain	YES NO YES with exemption
	ings, wells, and surface water information How many springs are within 100 m of manua facilities or manure collection areas?		0	None identified on site visit	YES NO
b.	How many water wells are within 100 m of th storage facilities or manure collection areas?	e manure	1 10 115735	WW ID 115735 21 m to East Barn	YES X*NO
c.	What is the shortest distance from an manure storage facility to a surface water body? (ie, l slough, seasonal, etc.)		1.3 Lem Imination canal	1.34 km to irrigation canal	YES INO YES with exemption
Groundwater information a. What is the depth to bedrock?		Estimated vieasured Drilling reports	29 m (95 ft from ww 115735 drillir report)		
c.	What is the shallowest depth to the uppermost groundwater resource?	<u>74 (</u> m)	Estimated Measured Drilling reports	2.7 m see UGR report	Unknown YES NO

Additional information: (attach borehole logs and records, as required)

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AO: Water well ID 115735 is located in the middle of the farmyard. North of Hog Barn 1 (East Barn), West of the open feedlot pens and South of the proposed covered pens. Water well log is attached.

* - A variance will be required for proposed facilities which have already been constructed.



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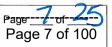
GENERAL WATER INFORMATION -	NRCB USE ONLY			
Use the proposed manure storage facil common body of water or water well	Comments	Meets regulations		
Proposed facility name Ane & L AQ: Under cover and op				
Flood plain information What is the elevation of the floor of the lowest proposed manure storage or collection facility above the 1:25 year flood plain or the highest known flood level?	<u>+1(</u> m)	Estimated	Not in known flood plain	YES INO
 Springs, wells, and surface water information a. How many springs are within 100 m of program storage facilities or manure collection areas 	O	None observed during site visit	YES INO	
 How many water wells are within 100 m of p manure storage facilities or manure collection 		1	WW ID 115735	YES X NO
c. What is the shortest distance from a <u>propos</u> collection or storage facility to a surface wat lake, creek, slough, seasonal, etc.)		1.2 hm	1.26 km from irrigation canal	YES NO
Groundwater information a. What is the depth to bedrock?	_ 29 (m)	Estimated	29 m (95 ft) per ww N/A 115735 drilling report	
b. What is the depth to the water table?	<u>, 4 (</u> m)	Estimated Measured Drilling reports	2.7 m in soils drilling report	YES NO YES with exemption
c. What is the shallowest depth to the uppermost groundwater resource?	<u>]4</u> (m)	Estimated Measured Drilling reports	2.7 m see UGR report	YES WITH Exemption

Additional information: (attach borehole logs and records, as required)

* - May meet 1 m above water table requirement, but has not provided sufficient information to show that

they can meet AOPA liner requirements or have a naturally occurring protective layer.

** - Because liner has not been shown to meet requirements





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GENERAL WATER INFORMATION -	NRCB USE ONLY			
Use the proposed manure storage facil common body of water or water well	Comments	Meets regulations		
Proposed facility name <u>Calch</u>				
Flood plain information What is the elevation of the floor of the lowest proposed manure storage or collection facility above the 1:25 year flood plain or the highest known flood level?	_ (m)	Estimated	Not in known flood plain	YES INO
 Springs, wells, and surface water informati a. How many springs are within 100 m of prop storage facilities or manure collection areas 	0	None observed during site visit	YES INO	
b. How many water wells are within 100 m of a manure storage facilities or manure collection		1	WW ID 115735 is located more than 100 m away.	YES INO YES with exemption
c. What is the shortest distance from a <u>propo</u> collection or storage facility to a surface was lake, creek, slough, seasonal, etc.)		1.3 hm	1.3 km to irrigation canal	YES NO YES with exemption
Groundwater information a. What is the depth to bedrock?	Estimated Measured Drilling reports	A shallow quarry is located just east of the catch basin site, indicative of shallow bedrock		
b. What is the depth to the water table?	<u>₩4</u> _(m)	Estimated Measured	Less than 2.7 m from surface based on soil drilling report	YES WITH exemption
c. What is the shallowest depth to the uppermost groundwater resource?	<u>#</u> (m)	Estimated Measured Drilling reports	Approx 2.7 m - see UGR report	YES X NO

Additional information: (attach borehole logs and records, as required)

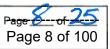
AO: The applicant requested to increase the size of the proposed catch basin on November 17, 2020 to 36 m x 25 m x 1.8 m deep.

* - The natural ground level of the catch basin is lower than the natural ground level of test hole AM4-19. It is therefore unlikely that the bottom of the catch basin can meet the 1 m water table separation requirement.

If approved following review a leakage detection monitoring system and condition relating to the shallow water table should be considered.

Last updated: 08 Jan 18

NRCB USE ONLY





Water Well Drilling Report

View in Metric Export to Excel

GIC Well ID

115735

GoA Well Tag No. The driller supplies the data contained in this report. The Province disclaims responsibility for its Drilling Company Well ID accuracy. The information on this report will be retained in a public database GOWN ID Date Report Received 1982/12/14 Well Identification and Location Measurement in Imperial Owner Name Address Town Postal Code Province Country HAWTHORNE, WAYNE P.O. BOX 1251 CLARESHOLM SEC TWP 1/4 or LSD RGE W of MER Block Additional Description Location Lot Plan 15 10 9 27 4 GPS Coordinates in Decimal Degrees (NAD 83) Measured from Boundary of Elevation Latitude 49.725817 Longitude -113.578252 ft ft from How Location Obtained How Elevation Obtained ft from Map Not Obtained **Drilling Information** Type of Work Method of Drilling Rotarv New Well Proposed Well Use Domestic & Stock Formation Log Measurement in Imperial Yield Test Summary Measurement in Imperial Recommended Pump Rate 0.00 igpm Depth from Water Lithology Description ground level (ft) Water Removal Rate (igpm) Static Water Level (ft) Bearing Test Date 40.00 Brown Till 1982/09/20 16.00 62 00 75.00 Blue Clay Well Completion Measurement in Imperial Total Depth Drilled Finished Well Depth Start Date End Date 95.00 Hard Shale & Gravel 95.00 ft 1982/09/20 1982/09/20 **Borehole** Diameter (in) From (ft) To (ft) 0.00 0.00 95.00 Surface Casing (if applicable) Well Casing/Liner Steel Steel Size OD : 7.00 in Size OD : 4.50 in 0.000 in 0.188 in Wall Thickness : Wall Thickness : Bottom at : 6.00 ft Top at : 0.00 ft Bottom at : 95.00 ft

Perforations

From (ft)

80.00

Perforated by

Screen Type

Pack Type

Amount

Annular Seal Driven Placed from

Amount Other Seals

Size OD :

From (ft)

Attachment _ Top Fittings

To (ft)

95.00

Type

Torch

Contractor Certification

Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER

Company Name HENNING DRILLING LTD. Certification No

Copy of Well report provided to owner Date approval holder signed

Slot Length

(in)

6.00 ft

Bottom Fittings

Grain Size

Diameter or

Slot Width(in)

0.188

0.00 ft to

0.00 in

To (ft)

Hole or Slot

Interval(in)

5.00

Slot Size (in)

At (ft)



Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

GoA Well Tag No.

View in Metric Export to Excel

Drilling Company Well ID

GIC Well ID

115735

GOWN ID			Date Repo	rt Received 1982/12/14
Well Identification and Location				Measurement in Imperia
	ddress O. BOX 1251 CLARESHOLM	Town	Province	Country Postal Code
	TWP RGE W of MER 9 27 4	Lot Block Pl	an Additional Descript	ion
Measured from Boundary of ft from ft from		nates in Decimal Degrees (N 19.725817 Longitude n Obtained	-113.578252 Elevation	ft
Additional Information				Measurement in Imperia
Distance From Top of Casing to Ground Is Artesian Flow Rateig			stalled	
Recommended Pump Rate Recommended Pump Intake Depth (Fro.	0.00 igpm m TOC) 80.00 ft	Pump Installed Yes	Depth Make	ft H.P5 Dutput Rating)
Did you Encounter Saline Water (>400 Additional Comments on Well DRILLER REPORTS WATER IS SOFT.		7 <u>ft</u>	Il Disinfected Upon Completior Geophysical Log Taken Submitted to ESRD ed for Potability	
Yield Test			Taken From Ground Lev	
Test Date Start Time 1982/09/20 12:00 AM	Static Water Level 62.00 ft	Pumping	(ft) Elapsed Time Minutes:Sec	e Recovery (ft)
Method of Water Removal Type Bailer Removal Rate 16.0 Depth Withdrawn From 62.0 If water removal period was < 2 hours, e	0 ft			
Water Diverted for Drilling				
Water Source	Amount Taken	g	Diversion Date & Ti	me

Contractor Certification		
Name of Journeyman responsible	for	d

rilling/construction of well UNKNOWN NA DRILLER

Company Name HENNING DRILLING LTD.

Certification No 1

Copy of Well report provided to owner Date approval holder signed

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WELL INFOR	MATION:							
Well IDs:	Well IDs: <u>115735</u>							
	See UGR report at the end of this document for shallow water well information.							
		rectly affected parties or refe	· · · · · · · · · · · · · · · · · · ·	res 🗖 NO				
	Ground water related concerns from directly affected parties or referral agencies: X YES NO Water Wells AO. WW variance required to be applied for because facilities already constructed							
		equired to be applied for ance requirements applied:		lition required: X*YES INO				
Surface Water		* - If appi		onitoring should be considered				
If applicable, exer	mption for 30 m dista	nce requirements applied:	🗆 YES 🔀 NO Conc	lition required: 🛛 YES 🛛 NO				
ERST for propose	ed facilities							
Fa	acility	Groundwater score	Surface water score	File Number				
Covered Pe	ens	82.8 Moderate	15 Low	LA19036				
Open Pens	3	80.4 Moderate	20 Low	LA19036				
Catch Basin		63.8 Low	20 Low	LA19036				
Moderate	e risks will need to	be addressed by the a	pplicant. See next pag	e.				
ERST for existing	g facilities							
Fa	acility	Groundwater score	Surface water score	File Number				
East Hog	Barn	90 Moderate	25 Low	LA19036				
West Hog	l Barn	90 Moderate	25 Low	LA19036				
East EMS	East EMS 95.7 High 30 Low LA19036							
West EM	West EMS 95.7 High 30 Low LA19036							
High and	Moderate risks w	ill need to be addressed	l - see next page					
Groundwater or	surface water relat	ted comments, see next p	age					

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Groundwater or surface water related comments:

The soil drilling logs indicate shallow groundwater in the area of the pens and catch basin. Just east of the catch basin the land owner has dug a shallow pit from which they are extracting and crushing rock for use at their operation. This is indicative of shallow bedrock.

The east and west EMS's appear as holes dug in the ground. The east EMS had liquid manure in the bottom. The west EMS appeared to have only water in the bottom. The operator did not have any information related to their construction. The bottom of the EMS's are approximately at the same depth as the UGR and water table.

The condition of the concrete liners in the underfloor pits of the two existing barns are unknown. The barns were constructed some time before 2001, possibly as early as the early 1980's. I did not enter the barns as they had livestock and manure in them for biosecurity reasons and because the liners would not be readily visible.

The roller compacted concrete (RCC) proposed, and already constructed, as a liner for the under cover and open pens has not been shown to be able to meet AOPA groundwater protection requirements.

I enlisted the assistance of Scott Cunningham, an environmental specialist with the NRCB, to assist with the ERST scoring. Detailed information used for the ERST scoring is contained in the ERST reports at the end of this document for ease of reference. The ERST results are in the tables above and the scoring sheets are on file.

Moderate and high risks to groundwater will need to be addressed by the applicant irrespective of whether a permit is issued.



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DISTANCE OF ANY MANURE STORAGE FACILITY (EXISTING OR PROPOSED) TO NEIGHBOURING RESIDENCES

Legal Land Description	Distance (m)	Zoning (LUB) Category	MDS Cat (1-4)	Distance (m)	Meets Regulations
SE=15-9-27 44	901) M	RG	1	920	Yes
10 SALA-H-9-27.WA	900 M	RG	1	925	Yes
55-10-9-27-64	500 M	RG	1	502	Yes
NW-10-9-27- W4	900 m	RG	1	900	Yes
54-10-9-27-24	ROOM	RG	1	1171	Yes
NE-15.9-27 WY	900m	RG	1	980	Yes
	SE-15-9-27 W4 10 SE-15-9-27 W4 SE-10-9-27-W4 NW-10-9-27- W4	(m) SE=15-9-27 W4 900 M MU-14-9-27 W4 900 M SE-10-9-27-W4 500 M NW-10-9-27-W4 900 M SW-10-9-27-W4 1200 M	(m) (LUB) Category SE - 15 - 9 - 27 44 90) M RG SE - 10 - 9 - 27 - 44 900 M RG NW - 10 - 9 - 27 - 44 900 M RG SU - 10 - 9 - 27 - 44 900 M RG SU - 10 - 9 - 27 - 44 900 M RG	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	(m)(LUB) Category(1-4)(m) $SE = 15 - 9 - 27 \ Ly4$ 90) MRG1920 $SE = 15 - 9 - 27 \ Ly4$ 90) MRG1925 $SE - 10 - 9 - 27 - 144$ 500 MRG1502 $NW - 10 - 9 - 27 - 144$ 940 MRG1900 $SU - 10 - 9 - 27 - 144$ 1200 MRG11171

Methods used/margins of error to determine distance:

Additional information:

RG = Rural general

NRCB USE ONLY	STATES OF A PARK OF A PARK OF A PARK OF	
Methods used to determine distance (if app +/- 5 Margin of error (if applicable):		
Requirements: Category 1:367 m	Category 2: 489 m Category 3: 612 m	Category 4: 979 m
Technology factor:	TYES NO	
Expansion factor:	TYES INO	
Waivers required:	□YES ♀NO #	
Waivers attached:	Waivers in file:	
MDS related concerns from directly affected	l parties or referral agencies:	5 □NO
Comments:		
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Name
Address
Legal Land
Location

MDS Spreadsheet based on 2006 AOPA Regulations

Category of Livestock	Type of Livestock	Factor A	Technology Factor	MU	LSU Factor	Annau Annau	LSU
Beef	Cows/Finishers (900+ lbs)	0.700	0.700	0.910	0.446		-
	Feeders (450 - 900 lbs)	0.700	0.700	0.500	0.245		-
	Feeder Calves (<550 lbs)	0.700	0.700	0.275	0.135	3,050	404.3
		0.000		0.000			-
Dairy	*Free Stall - Lactating Cows with all associated dries, heifers, and calves	0.800	1.100	2.000	1.760		-
(*count	*Free Stall - Lactating cows with Dry Cows	0.800	1.100	1.640	1,443		
actating	only	0.000	1.100				
cows only)	Free Stall - Lactating Cows only	0.800	1.100	1.400	1.232		-
	Tie Stall - Lactating cows only	0.800	1.000	1.400	1.120		-
	Loose Housing - Lactating cows only	0.800	1.000	1.400	1.120		•
	Dry Cow (Solid manure)	0.800	0.700	1.000	0.560		-
	Dry Cow (Liquid manure) Replacements - Bred Heifers (Breeding to	0.800	0.700	0.875	0.490		
	Calving)	0.000	0.700	0.075	0.450		-
	Replacements - Growing Heifers (350 lbs to	0.800	0.700	0.525	0.294		-
	breeding)						
	Calves (< 350 lbs)	0.800	0.700	0.200	0.112		-
Outra-	Columnia Arrish *	0.000	1.000	4 700	0.040		-
Swine Liquid	Farrow to finish * Farrow to wean *	2.000	1,100	1.780	3.916		-
Liquia (*count	Farrow to wean *	2.000	1.100	0.670	1.474	-	-
sows only)	Feeders/Boars	2.000	1.100	0.200	0.440		-
00110 011197	Growers/Roasters	2.000	1.100	0.118	0.260		
	Weaners	2.000	1.100	0.055	0.121		-
	Rever and the second second second			1000			-
Swine	Farrow to finish *	2.000		1.780	2.848		-
Solid	Farrow to wean *	2.000	0.800	0.670	1.072		-
(*Count	Farrow only *	2.000	0.800	0.530	0.848		-
sows only)	Feeders/Boars	2.000	0.800	0.200	0.320		-
	Growers/Roasters Weaners	2.000	0.800	0.118	0.189		· ·
	Weatiers	2.000	0.800	0.055	0.066		
Poultry	Chicken - Breeders - Solid	1.000	0.700	0.010	0.007		
,	Chicken - Layers - Liquid (includes	2.000	1.100	0.008	0.018		-
	associated pullets)						
	Chicken - Layers - (Belt Cage)	2.000	0.700	0.008	0.011		-
	Chicken - Layers - (Deep Pit)	2.000	0.700	0.008	0.011		-
	Chicken - Pullets/Broilers	1.000	0.700	0.002	0.001		-
	Turkey - Toms/Breeders	1.000	0.700	0.020	0.014		
	Turkey - Hens (light) Turkey - Broilers	1.000	0.700	0.013	0.009		-
	Ducks	1.000	0.700	0.010	0.007		
	Geese	1.000		0.020	0.014		
	Other Processing on the Excellence						
Horses	PMU	0.650	0.700	1.000	0.455		-
	Feeders > 750 lbs	0.650	0.700	1.000	0.455		-
	Foals < 750 lbs	0.650	0.700	0.300	0.137		-
	Mules	0.600	0.700	1.000	0.420		
	Donkeys	0.600	0,700	0.670	0.281	-	
Sheep	Ewes/Rams	0.600	0.700	0.200	0.084		-
Sneep	Ewes with lambs	0.600		0.200	0.084		
	Lambs	0.600		0.050	0.021		
	Feeders	0.600		0.100	0.042		-
	Ditter						-
Goats	Meat/Milk (per Ewe)	0,700		0.170	0.083		-
	Nannies/Billies	0.700		0.140	0.069	_	-
	Feeders	0.700	0.700	0.077	0.038		-
Diser	Piece	0.000	0.705	1.000	0.400		-
Bison	Bison	0.600	0.700	1.000	0.420	-	
Cervid	Elk	0.600	0.700	0.600	0.252	-	
Cervia	Deer	0.600		0.800	0.252		
	Citing and a second second	0.000	0.700	0.200	0.004		-
Wild Boar	Feeders	2.000	0.800	0.140	0.224		
				0.371	0.594		-
	Sow (farrowing)	2.000	11.00011				

For New Operations Dispersion Factor

404.3

Total

		Distance		
Category	Odour Objective	Feet	Metres	
1	41.04	1,204	367	
2	54.72	1,605	489	
3	68.4	2,007	612	
4	109.44	3,211	979	

For Expanding Operations Dispersion Factor Expansion Factor

1
0.77

1

		Dista	nce
Category	Odour Objective	Feet	Metres
1	41.04	927	283
2	54.72	1,236	377
3	68.40	1,545	471
4	109.44	2,472	754





Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

LAND BASE FOR MANURE AND COMPOST APPLICATION (for approvals and registrations only)

Name of landowner(s)*	Legal Land Description	Area ** (usable hectares)	Soil Zone	NRCB USE ONLY Area unsuitable:
Ane & W. Hemich Mulinih	NE-10-9-27-W4	150 55	Park Brown	136 ac DB drylar
Nico & Conien De U.J	SE-15-9-27-64	NSC: 6-0-63	Injoted Dade Book	155 irrig ac per agreement
	TOTAL			

*If you are **not** the registered land owner, please attach copies of land use agreements signed by all landowners.

** Available manure spreading area (do not include required setback areas from residences, common bodies of water, water wells, etc.) (to convert from acres to hectares divide acres by 2.47)

Additional information: (attach copies of all signed land use agreements)

See attached

NRCB USE ONLY							
Land base required: 45ha (111 ac) irrigated or 93ha (230 ac) dark brown (dryland)							
Land base listed:	se listed: 63 ha (155 ac) irrigated & 55 ha (136 ac) dark brown (dryland)						
Area not suitable:							
Available area	Greater tha	n required		Requirement Met:		🛛 YES 🗆 NO	
Land spreading agreements	required:	X YES NO	If yes,	Agreements in file	. 🗆	Agreements attached:	¥1
Manure Management Plan:				Plan attached:		Plan in file:	
					10.55		

	- 11
NRCB USE ONLY	Pageof Page 15 of 100
	NRCB USE ONLY

Manure Spreading Agreement

Nico De With agree to allow Arie Mullwith (applicant) to spread manure on the following fields during _______ (calendar year).

Land location	Acres	Suitable for spreading	Soil zone
SE-15-9-27- W4	155	55	Inighted Darh Brown
			•
	λ.		

Signed: N-CA- de Wil

Date: _____

AO: If following a review hearing a permit is granted, a new manure spreading agreement will be required since this one is only valid for 2020.

Landbase Requirements (hectares) based on 2006 AOPA requirements

Category of Livestock		Number of Animals	Dark Brown & Brown (ha)	Grey Wooded (ha)	Black (ha)	Irrigated (ha)
Beef	Cows/Finishers (900+ lbs)	0	0	0	0	(
	Feeders (450 - 900 lbs)	0	0	0	0	
	Feeder Calves (<550 lbs)	3000	93.000	78.000	57.000	45.000
		0			-	
Dairy	*Free Stall – Lactating Cows with all associated dries, heifers, and calves	0	0	0	0	(
*count	*Free Stall – Lactating cows with Dry Cows	0	-	-		
actating	only		-	-	-	
cows only)	Free Stall - Lactating Cows only	0	-	-	-	-
50113 011y)	Tie Stall - Lactating cows only	0	-	-	0	
	Loose Housing - Lactating cows only	0	-	-	-	-
	Dry Cow (Solid manure)	0	-	-	-	-
	Dry Cow (Liquid manure)	0	-	-	-	
	Replacements - Bred Heifers (Breeding to	0	-	-	-	-
	Calving) Replacements - Growing Heifers (350 lbs to breeding)	0	-	-	-	-
	Calves (< 350 lbs)	0	-	-	-	-
	Officer and the local sector of the Sciences	0				
Swine	Farrow to finish *	0	-	0	-	-
Liquid	Farrow to wean *	0		-	-	-
(*count	Farrow only *	0			-	-
sows only)	Feeders/Boars	0		0	0	
	Growers/Roasters	0		-	-	-
	Weaners	0	· ·	-	-	-
Swine	Forrow to finish *	0			-	-
Solid	Farrow to finish * Farrow to wean *	0		-	-	
(*Count	Farrow only *	0	· ·		-	-
sows only)	Feeders/Boars	0			-	-
SOWS Only/	Growers/Roasters	0			-	-
	Weaners	0		-	-	-
		0				
Poultry	Chicken - Breeders - Solid	0	-	-	-	-
,	Chicken - Layers - Liquid (includes associated pullets)	0	-	0	0	
	Chicken - Layers - (Belt Cage)	0	-	-	-	-
	Chicken - Layers - (Deep Pit)	0	-	-	-	-
	Chicken - Pullets/Broilers	0	-	0	0	
	Turkey - Toms/Breeders	0	0	0	0	
	Turkey - Hens (light)	0	-	-	-	-
	Turkey - Broilers	0	- 0	-	-	-
	Ducks	0	0	0	0	
	Geese	0		0	0	
Horses	PMU	0	0	0	0	
1101363	Feeders > 750 lbs	0		0		-
	Foals < 750 lbs	0	-	-	-	-
	Mules	0	-	-	-	
	Donkeys	0	-	-	-	-
	Other Inc. States of the Antibular States	0				
Sheep	Ewes/Rams	0	-	0	0	
	Ewes with lambs	0	-	-	-	-
	Lambs	0	-	-	-	-
	Feeders	0	-	-	-	-
	Construction of the second second second	0				
Goats	Meat/Milk (per Ewe)	0	0	1	0	
	Nannies/Billies	0	· ·	-	-	-
	Feeders	0	-		-	-
Bison	Bison	0	0	0	0	
Convid		0		-	0	
Cervid	Elk		0			
	Deer	0	0	0	0	
Wild Boar	Feeders	0	-	0	0	
wing post	Feeders Sow (farrowing)	0		-	-	-
	Cow (lanowing)	0	+			
	Total Hectares		93.0	78.0	57.0	45
	Total Acres		229.8	192.7	140.8	111



Technical Document

NRCB Natural Resources Conservation Board

Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

ALL SIGNATURES IN FILE:

XYes No

DATES OF APPROVAL OFFICER SITE VISITS:	
September 17 2019 (previous approval officer)	November 4 2020

CORRESPONDENCE WITH MUNICIPALITIES AND REFERRAL AGENCIES:					
Date deeming letters sent _	Oct 9 2019				
Municipality:MD @	of Willow Creek				
Letter sent	Response received	written/email	Verbal	no comments received	
Alberta Health Services:					
Letter sent	Response received	written/email	Verbal	no comments received	
Alberta Environment and	Parks: N/A	N			
Letter sent	Response received	written/email	□verbal	no comments received	
Alberta Transportation:	□ N/A	ι.			
Letter sent	Response received	written/email	Verbal	no comments received	
Alberta Regulatory Servic	es: 🛛 N/A	N			
Letter sent	Response received	□written/email	□verbal	no comments received	
Other: Lethbridge Not	thern Irrigation Dist	rict			
Letter sent	Response received	Wwritten/email	□verbal	no comments received	
Other:					
Letter sent	Response received	□written/email	Dverbal	no comments received	

Technical Document



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

PLANS	
Submitted and attached construction plans	
Submitted aerial photos	X YES INO
Submitted photos	TYES INO

GRANDFATHERING:	
•	Yes No randfathered (deemed) capacity and facilities was carried out as part of lication. See appendix E in decision summary for details
On a previous application/decision: Comments:	Yes X No I yes, list application/decision number
Approval LA10054M included a "grand correcting an error with the capacity an	fathered capacity" for the CFO, however, LA10054N superseded LA10054M, Id not listing any capacity for the CFO.
DEEMING CAPACITY: Comments:	XYes No
The east hog barn had feeder ca primarily being used to store thin	hange from hogs to feeder calves occurred approximately 8 years ago. lves in it on the date of my site inspection. The west hog barn was gs for the operation. The operator did indicate that they had a few f my site inspection. (The proposed pens and shelter were also the date of my site inspection)



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

SOLID MANURE, COMPOST & COMPOSTING MATERIALS: Barns, feedlots & storage facilities -Alternative liner

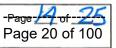
(complete a copy of this section for **EACH** barn, feedlot and storage facility for solid manure, composting materials or compost with a alternative liner)

Facility description / name (as indicated on site plan)

Open pen	$\frac{1}{5}$	arrals)	2. <u></u>	Shelter
Manure storage capacity Under cover pens				
Lengt	n (m)	Width (m)	Estimated storage capacity (m ³)	Depth below grade to the botton of the liner (m)
· 92m		37 m	NA	0
m 58		15 m	N AI	0
RCB USE ONLY epth to water ta epth to UGR:	ble: 2. <u>7 -</u> 2.7 - 3	3.0 m from drilling rep 3.0 m from drilling rep res □ NO	oort	es 🕅 no
RST completed:		oderate		
* - Applicant	has not de	monstrated that the	Surface Water risk leve liner being proposed can mee r AOPA's Standards and Administratio	t AOPA requirements
Outdoor:	f: Surface wa Describe the r	er will be controlled by the	e walls and roof of the building and b system proposed for feedlots and outc G 100 F	
RCB USE ONL Requirements me See next pac	et: 🗆	YES 🗆 NO	Details/comments:	

Last updated: 05 Feb 18

NRCB USE ONLY





Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

SOLID MANURE, COMPOST & COMPOSTING MATERIALS: Barns, feedlots & storage facilities - Alternative AO: This information does not show how AOPA requirements are met. Applicant provided a report from Wood Environmental and Infrastructure solutions (Wood) dated Oct. 29, 2020,

Alternative liner details updated on Nov 6, 2020to show how AOPA requirements are addressed

a. Describe the proposed alternative liner Poller compacted Concrete liner	Provide details: 6"-7" of poller compacted concrete to make a durable liner, professionally inshalled
b. Information and calculations used to show equivalency	Provide details:

Additional information:

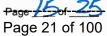
AO: The proposed alternative liner information in the application is not sufficient to show if AOPA groundwater protection requirements can be met. The RCC floor was placed in the Fall of 2019, prior to a permit being issued. The applicant was asked to provide information to show how what they proposed and constructed can meet AOPA requirements. Copies of soil drilling tests and a report prepared by Wood dated Oct. 29, 2020 and updated on Nov 6, 2020 was provided. This report provides information from tests which were carried out in June 2020 - approx. 7 months after the RCC had been installed. I note that the Engineer was not on site when the ground was prepared nor when the RCC was placed.

No information was provided from the contractor who installed the RCC.

The RCC floors in both the covered and open pens were covered with manure and bedding and not visible at the time of my site inspection in November 2020.

NRCB USE ONLY Liner requirements met:		Condition required:	
Comments:			
	OPA groundwater protect	demonstrate that the propo tion requirements. Details a	

Last updated: 05 Feb 18



NRCB USE ONLY



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

RUNOFF CONTROL CATCH BASINS: Synthetic liner (complete a copy of this section for EACH manure storage facility with a synthetic liner) Facility description / name (as indicated on site plan) Aun - off (atch basin 2. 3. Determination of minimum required catch basin volume Show your calculations for Provide details:

Show your calculations for determining the minimum required	Provide details:	
catch basin volume	see attached	

Catch basin capacity

					Slope run:rise			Depth below
	Length (m)	Width (m)	Depth (m)	Inside end walls	Inside side walls	Outside walls	Estimated storage capacity (excl. freeboard) (m ³)	grade of the bottom of the synthetic liner (m)
1.	-25-	-17-	1.5	3	3		212	
2.	36	21	1.8 applicant N		d dimension	s as per	540	approx 1.8 m
3.		;	applicant r	17, 20				
L	I		1	L	тот	AL CAPACITY	540	

NRCB USE ONLY		State and a state of the			
Catch basin calculator	(calculation attached). Total volume (@ freeboard level 540 m	³ Requirements met:	X YES NO	
Depth to water table:	less than 2.7 m*	Requirements met:	YES X NO		
Depth to UGR:	less than 2.7 m* based on	Requirements met:	YES X*NO		
	ERST support information				
ERST completed:	I YES I NO				
Groundwater risk level	·	Surface Water I	risk level:		
* Top of catch basin is lower than surface level of test hole AM4-19 therefore water table will be shallower than 2.7 m UGR: Uppermost Groundwater Resource as defined under AOPA's <i>Standards and Administration Regulation</i> .					
Last updated: 05 Feb 18				16 25	
	NF	CB USE ONLY		Page 22 of 100	



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

RUNOFF CONTROL CATCH BASINS: Synthetic liner (cont.)

Synthetic liner details			
a. Synthetic liner	Thickness and type of liner material :	Provide liner material details:	
flope 40	40 mil	See attached	
Additional information:	ана Балана нада дана де "		
NRCB USE ONLY			
Liner requirements met: Comments:	X YES 🗆 NO	Condition required: X YES] NO
Catch basin liner can	meet AOPA GW protection	requirements,	
however, condition re	equiring completion report w	ill be required	
Leakage detection system re	equired: X YES NO	If yes, please explain why.	
Comments: 4.4 m which than the top is likely that of this, if a pe table must a	is saturated below 2.7 m. B of the proposed catch basin the catch basin will be const ermit is issued, a leakage de lso be verified at the time of	surface to 1.0m, very fine sandy loar secause the ground surface at the te and the catch basin is proposed to rructed into or very close to the wate etection system will be required. The construction to ensure AOPA requi	st hole is higher be 1.8 m deep, it r table. Because e depth to water
if a permit is Construction plans approved		TYES 🛛 NO	
Installed by approved contra Preparation of liner bed (cor		X YES INO	
basin and ir	nstallation of the synthetic carried out in accord	required to ensure the constructi liner, and the installation of a le ance with engineering and line	akage detection
			17.75
Last updated: 05 Feb 18	NRC	B USE ONLY	Page 1-7 of Page 23 of 10

NRCB USE ONLY



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

RUNOFF CONTROL CATCH BASIN:	Synthetic liner (cont.)						
NRCB USE ONLY							
Catch basin calculator total volume @ freeboard level: <u>540 m</u> ³ Runoff capacity requirements met: X YES NO							
Calculation of the volume attached: \mathbf{X} YES	□ NO						
Depth to water table: Less than 1 m based on soil test hole information. Requirements met: YES X NO							
Depth to Uppermost Groundwater Resource:	Depth to Uppermost Groundwater Resource: Less than 1 m based on soil test hole results Requirements met:						
ERST completed: 🛛 See details in ERST pag	je						
Liner requirements met: Comments: See comments below.	🖾 yes 🗖 no	Condition	n required:	X YES D NO			
Leakage detection system required:	X YES NO If yes	, please exp	lain why.				
Proximity of the water table and UGR require a	leakage detection system to be inst	alled.					
Construction plans approved by professional	engineer:						
Will liner be installed by manufacturer approv	ved contractor and qualified third	d party?:					
Condition required:			🛛 YES 🗖 NO				
Preparation of liner bed (comments):							
Preparation of liner bed needs to be in accordance with the liner manufacturer's requirements. Installation of synthetic liner needs to be supervised and in accordance with liner manufacturer's requirements. A leakage detection system will need to be installed.							

Catch Basin Calculator

m m m run:rise run:rise m ³	-	Feet Feet Feet run:rise run:rise ft ³	Name ₁ Land Location ₁ Area ₂ Length 1 2 3 4 5 Total Au Select Town ₃ Fort Macleod 90 Design Rainfall	92 37 rea =
m m run:rise run:rise m ³	68.90 5.91 4.27 3 3 30,962 192,857	Feet Feet run:rise run:rise ft ³	Land Location ₁ Area ₂ Length 1 2 3 4 5 Total A Select Town ₃ Fort Macleod 90	(m) Width (m) A 92 37 rea
m m run:rise run:rise m ³	5.91 4.27 3 3 30,962 192,857	Feet Feet run:rise run:rise ft ³	Area ₂ Length 1 2 3 4 5 Total Ar Select Town ₃ Fort Macleod 90	(m) Width (m) A 92 37 rea
m run:rise run:rise m ³	4.27 3 3 30,962 192,857	Feet run:rise run:rise ft ³	1 2 3 4 5 Total A Select Town ₃ Fort Macleod 90	92 37 rea
run:rise run:rise m ³	3 3 30,962 192,857	run:rise run:rise ft ³	2 3 4 5 Total A Select Town ₃ Fort Macleod 90	rea
run:rise m ³	30,962 192,857	run:rise ft ³	3 4 5 Total A Select Town ₃ Fort Macleod 90	
m ³	30,962 192,857	ft ³	4 5 Total A Select Town ₃ Fort Macleod 90	
	192,857		5 Total Ar <mark>Select Town</mark> 3 Fort Macleod 90	
	192,857		Total An Select Towr ₃ Fort Macleod 90	
	192,857		Select Town ₃ Fort Macleod 90	
	192,857		Fort Macleod 90	
	192,857		Fort Macleod 90	
	192,857			
Capacity		Imp. Gal.	Design Rainfall	
Capacity				90 n
run:rise	3 3	Feet run:rise run:rise	Catch Basin Minim 306 m ³	num Design Storage 10,819 fi
	118.782	Imp. Gal.		67,390 li
m ²			** Actual storage vo	
			slightly greater than	design storage volun
	m run:rise m ³ m ²	run:rise 3 run:rise 3 m ³ 19,070 118,782	run:rise 3 run:rise run:rise 3 run:rise m ³ 19,070 ft ³ 118,782 Imp. Gal.	run:rise 3 run:rise run:rise 3 run:rise Catch Basin Minim m ³ 19,070 ft ³ 306 m ³ 118,782 Imp. Gal. m ² 6,394 ft ² ** Actual storage vo

Lines in Black - Catch basin dimension
 Lines in Blue - full level

25.2 m

10.2 m

18.0 m

NTS - Not Drawn To Scale

21.0 m



Our HDPE 40 geomembranes are designed in accordance with the Geomembrane Research Institute GM 13 standard. It is manufactured to meet the properties of GRI GM13 textured High Density Polyethylene and has been extensively used in a variety of containment applications. HDPE geomembranes have low permeability, good ultra violet resistance properties and excellent chemical resistance. HDPE 40 is a field assembled lining material that must be installed by trained installers. HDPE is used in a multitude of applications as a landfill liner, pond linings, and water containment projects.

Property	ASTM	HDPE 40 Textured ¹ Black Single Sided (SS)
Thickness nom. (min.avg)	D5994	40 mil (36 mil)
		1.00 mm (0.915 mm)
Thickness	D5994	
	Lowest Individual for 8 out of 10 values	36 mil/0.93 mm
	Lowest individual for any of the 10 values	34 mil/0.88 mm
Asperity Height (min.ave)	D 7466	16 mil
		0.4 mm
Sheet Density (minimum)	D792	≥0.940 g/cc
Dimensional Stability	D 1204	±2%
Tensile Properties (min. avg)	Tensile Strength @ Break	60 ppi
ASTM D 6693; Modified Type IV Die		10 kN/m
Gage length break: 2″ (50 mm)	Tensile Strength @ Yield	84 ppi
Gage length yield: 1.3" (33 mm)		15 kN/m
	Tensile Elongation @ Break	100%
	Tensile Elongation @ Yield	12%
Tear Resistance (min. avg)	D1004	28 lbs
		125 N
Puncture Resistance (min. avg)	D4833	60 lbs
		267 N
High Pressure Oxidative Induction Time (HPOIT)	D5885	400 mins
Stress Cracking	D5397	500 hrs
Carbon Black Content ¹	D1603	2.0-3.0 %
Carbon Black Dispersion ²	D5596	CAT 1 or 2
Oven Aging	D5721	80%
85° C, HPOIT retained after 90 days	D D5885	
UV Resistance- % HPOIT retained	D7238	50%
after 1600 hrs	D5885	
	Typical Roll Dimensions (Rolls dimensions may vary ± 1%)	
Roll Width	-	22.5 feet
		6.86 mtrs
Roll Length	n	780 feet

¹This product is designed and manufactured to meet the GRI GM13 specification

Disclaimer: Layfield disclaims any and all express, implied, or statutory standards, warranties or guarantees, including without limitation any implied warranty as to merchantability or fitness for a particular purpose or arising from a course of dealing or usage of trade as to any equipment, materials, or information furnished herewith. This document should not be construed as engineering advice.



Our HDPE 60 geomembranes are designed in accordance with the Geomembrane Research Institute GM 13 standard. It is manufactured to meet the properties of GRI GM13 and has been extensively used in a variety of containment applications. HDPE geomembranes have low permeability, good ultra violet resistance properties and excellent chemical resistance. HDPE 60 is a field assembled lining material that must be installed by trained installers. HDPE is used in a multitude of applications as a landfill liner, pond linings, and water containment projects.

Property	ASTM	HDPE 60 Textured ¹ Black Single Sided(SS)
Thickness nom. (min.avg)	D5199	60 mil (57 mil)
		1.5 mm (1.45 mm)
Thickness	D5199	
	Lowest Individual for 8 out of 10 values	54 mil/1.4 mm
	Lowest individual for any of the 10 values	51 mil/1.3 mm
Asperity Height (min.ave)	D 7466	16 mil
		0.4 mm
Sheet Density (minimum)	D792	≥0.940 g/cc
Dimensional Stability	D 1204	±2%
Tensile Properties (min. avg)	Tensile Strength @ Break	90 ppi
ASTM D 638; Modified Type IV Die		16 kN/m
Gage length break: 2" (50 mm)	Tensile Strength @ Yield	126 ppi
Gage length yield: 1.3" (33 mm)		22 kN/m
	Tensile Elongation @ Break	100%
	Tensile Elongation @ Yield	12%
Tear Resistance (min. avg)	D1004	42 lbs
		187 N
Puncture Resistance (min. avg)	D4833	90 lbs
		400 N
High Pressure Oxidative Induction Time (HPOIT)	D5885	400 mins
Stress Cracking	D5397	500 hrs
Carbon Black Content ¹	D1603	2.0-3.0 %
Carbon Black Dispersion ²	D5596	CAT 1 or 2
Oven Aging	D5721	80%
85° C, HPOIT retained after 90 days	D D5885	
UV Resistance- % HPOIT retained	D7238	50%
after 1600 hrs	D5885	
	Typical Roll Dimensions (Rolls dimensions may vary ± 1%)	
Roll Width	<u> </u>	22.5 feet
		6.86 mtrs
Roll Length	-	560 feet

¹This product is designed and manufactured to meet the GRI GM13 specification

Disclaimer: Layfield disclaims any and all express, implied, or statutory standards, warranties or guarantees, including without limitation any implied warranty as to merchantability or fitness for a particular purpose or arising from a course of dealing or usage of trade as to any equipment, materials, or information furnished herewith. This document should not be construed as engineering advice.

Mherta Transportation

Southern Region Box 314, 909 3 Avenue North Lethbridge, Alberta T1H 0H5 Telephone: 403-381-5426 Fax: 403-382-4057 www.alberta.ca/ministry-transportation.aspx

AT File Reference: RSDP027438 Our Reference: 2511-NE 10-9-27-W4M (785) Permit No. 5548-19

September 26, 2019

Arie and Willemiek Muilwijk awmuilwijk@hotmail.com Box 1628 Fort Macleod, AB TOL 0Z0

Dear Mr. and Mrs. Muilwijk:

RE: PROPOSED CALF SHELTER AND GRAIN SHED

Attached is a permit issued under the Highways Development and Protection Regulation, being Alberta Regulation 326/2009 and amendments thereto, authorizing the above noted development. This permit is subject to the conditions listed on page 2.

In consideration of Permit No. 5548-19, the applicant shall indemnify and hold harmless Alberta Transportation, its employees and agents, from any and all claims, demands, actions, and costs whatsoever that may arise, directly or indirectly, from anything done or omitted to be done in the construction, maintenance, alteration, or operation of the works authorized.

Issuance of this permit by Alberta Transportation does not relieve the holder of the responsibility of complying with relevant municipal bylaws, and this permit once issued does not excuse violation of any regulation, bylaw, or act that may affect this project.

Upon completion of the project, we ask that you notify Darren Davis, Assistant Development/Planning Technologist, or Leah Olsen, Development/Planning Technologist, at Lethbridge, 403-381-5426, who will inspect the conditions of the permit. Your cooperation in this matter is appreciated.

Yours truly,

Darren Davis Assistant Development/Planning Technologist

DD/jb

CC:

Municipal District of Willow Creek No. 26 – <u>chisholm@mdwillowcreek.com</u>; <u>brenda@mdwillowcreek.com</u>

Volker Stevin – <u>fortmacleod.admin@volkerstevin.ca</u> Rick Lemire – e-mailed Darren Davis – e-mailed

Page 28 of

M:\DS\SR\LETH\Development\Permits\Road Side Development\Muilwijk permit 5548-19 (RSDP027438).docx



(To be completed by Alberta Transportation)

ROADSIDE DEVELOPMENT APPLICATION APPROVAL FOR DEVELOPMENT NEAR A PRIMARY HIGHWAY

PERMIT

Permissio	on is hereby granted to	Arie and Willem	iek Muilv	vijk	to carry out the development in		
accordance with the plan(s) and specifications attached hereto and subject to the conditions shown below.							
If the dev	elopment has not been carried ou	t by the 26 th	day of	September	2020	this permit	
lapses and the applicant must reapply for a new permit if they wish to proceed.							
SIGNED	Pro Dun		PE	RMIT NO.	5548-19		
			FIL	E NO.	2511-NE 10	-9-27-W4M (785)	
TITLE	Assistant Development/Planning	Technologist	DA	TE	September	26, 2019	

PERMIT CONDITIONS: (Note: This permit is subject to the provisions of Section 11 – 19 inclusive of the Highways Development and Protection Act, Chapter H-8.5 2004, amendments thereto, and Highways Development and Protection Regulation (Alberta Regulation 326/2009) and amendments thereto).

- A. ACCESS CONDITIONS: (Note: All highway accesses are to be considered temporary. No compensation shall be payable to the applicant or his assigns or successors when the Department removes or relocates the temporary access or if highway access is removed and access provided via service road).
- 1. (a) No direct highway access will be permitted. Access shall be via the local municipal road.
 - (b) Use of the existing highway access may continue on a temporary basis.
 - (c) Permit authorizes construction of proposed access at the location shown and to the attached specifications. (Figure D-3.3b)
- 2. No additional highway access will be permitted.
- 3. The applicant shall construct and maintain any highway access to the Alberta Transportation's satisfaction.
- 4. Approval of companies having buried utilities shall be obtained prior to access construction or upgrading.
- **B. SETBACK CONDITIONS** (Note: Minimum setbacks usually allow for anticipated highway widening and construction of a service road parallel and adjacent to the highway).
- 1. The proposed <u>calf shelter and grain shed</u> is to be set back <u>77 meters (28 feet)</u> from the highway property line as shown on attached approved site plan.
- 2 The department accepts no responsibility for the noise impact of highway traffic upon any development or occupants thereof.

C. OTHER CONDITIONS:

- 1. This permit is issued subject to the approval of the Municipal District of Willow Creek No. 26.
- 2. This permit approves only the development contained herein, and a further application is required for any changes or additions.
- 3. The department is under no obligation to reissue a permit if the development is not completed before expiry of this permit.
- 4. Darren Davis, Assistant Development/Planning Technologist, or Leah Olsen, Development/Planning Technologist, in Lethbridge, telephone 403-381-5426, shall be notified before construction commencement.
- 5. The applicant shall not place any signs contrary to Alberta Regulation 326/2009. A separate "SIGN APPLICATION" form shall be submitted for any proposed sign.

D. ADDITIONAL CONDITIONS and/or ADVISEMENTS:

See attached Schedule "A"

SCHEDULE "A" Permit 5548-19

D: ADDITIONAL CONDITIONS and/or ADVISEMENTS:

- 1. This permit is approval for development of a calf shelter and grain shed only. Any additional development will be expressly subject to Condition C.2.
- 2. The applicant shall ensure that all on-site development, including ancillary development, is setback from the highway right-of-way boundary as shown on the attached approved site plan. Under no circumstance shall a different setback be implemented without the written permission of Alberta Transportation.
- 3. Further to condition A.1.(b), the department will not accept any responsibility for compensation requests/claims dealing with loss of business, inconvenient access, or any other disruption that may arise as result of the possible revision to the existing access arrangement. The possible revision to the existing access arrangement. The possible revision to the existing access arrangement may be due to access management/operational, construction, or planning activities carried out by the department or its consultants.
- 4. Further to Condition B.2, noise impact and the need for attenuation should be thoroughly assessed. The applicant is advised that provisions for noise attenuation are the sole responsibility of the developer and should be incorporated as required into the development of the property.
- 5. Any peripheral lighting (yard lights/area lighting) that may be considered a distraction to the motoring public or deemed to create a traffic hazard will not be permitted.

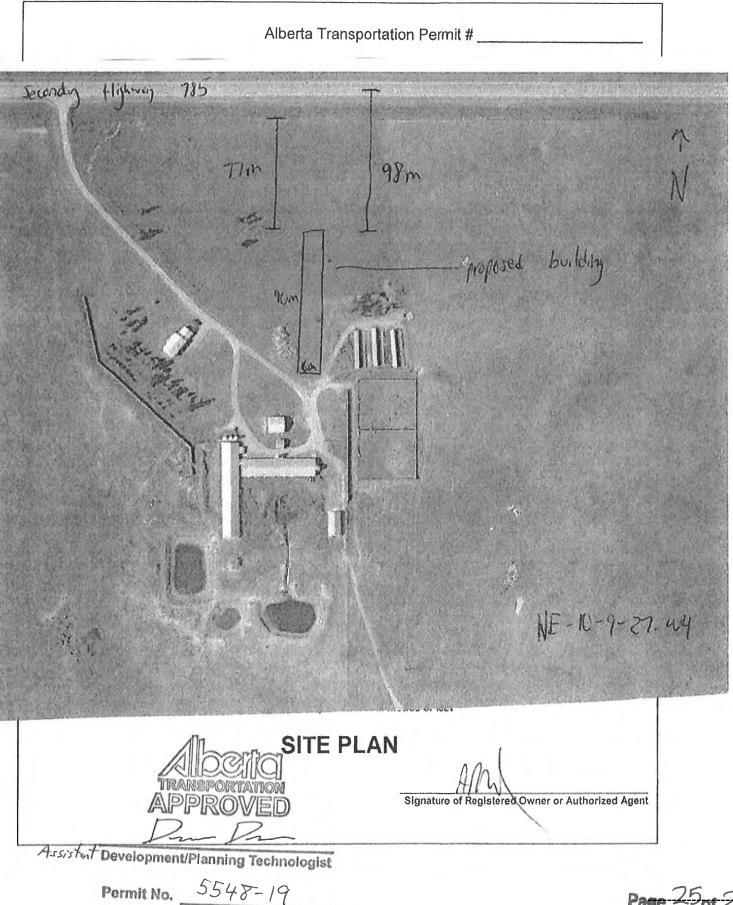
Government of Alberta Transportation Transportation ROADSIDE DEVELOPMENT APPLICATION FOR DEVELOPMENT NEAR A PROVINCIAL HIGHWAY

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In consideration of any perm employees and agents from or omlited to be done in the designated by Alberta Trans The issuance of a permit by and this permit once issued	nlt issued in respect t any and all claims, de construction, mainten portation to enter upor Alberta Transportatio	o this application emands, action ance, alteration in land for the p in does not relia	on, the Applica s and costs wh n or operation o urpose of inspe ave the holder o	nt shall indemn atsoever that m If the works aut ction during the of the responsit	ay arise, dire horized. The processing o	ctly or indirectly fro Applicant also con of this application, lying with relevant	om anything done sents to a person
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l(print full name)	hereby	certify that _	I am auth the ov	orized to act o wner's behalf	on	Signatu	re
and that the information give application for roadside deve	en on this form is full lopment.	press and a second	and is, to the t		(Date)	September.	. /
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Government **ROADSIDE DEVELOPMENT APPLICATION FOR DEVELOPMENT NEAR A PROVINCIAL HIGHWAY**

of Alberta 🔳 Transportation



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CHILAKO DRILLING SERVICES LTD

Box 942 Coaldale, Alberta, T1M 1M8 (403) 345-3710

SOIL PROFILE AND PARENT MATERIAL DESCRIPTION

Site Location: Arie Muilwijk

Date: 9-Aug-19

Hole #	Location	Depth		Moisture	Geological	Sample	Remarks
AM1-19	0314346	0-2.1	VFSL	SM	Lac		Silty
	5511364	2.1-3.5	VFSCL	VM	Lac		
		3.5-5.1	VFSL	VM-Sat			
		5.1-5.9	SiCL	М	Lac		V. firm, med-high plastic, yellow brown
		5.9-6.2	FSCL	VM	Lac		Slough @ 3.3m
4140 40	0044054				1		
AM2-19	0314354	0-2.9	VFSL	SM	Lac		Silty
	5511400	2.9-3.6	SiCL	VM	Lac		Sandy
		3.6-5.6	VFSL	Sat	Lac		Soft, olive brown, silty, free water
		5.6-6.2	SiCL	М	Lac		V. firm, med-high plastic, olive brown
							slough @ 3.9m
AM3-19	0314364	0-1.8	VFSL	М	Lac		Loose, olive brown, silty
7 1010-13	5511294	1.8-2.3	VFSCL	VM	Lac		Low plastic, olive brown, silty
	5011204	2.3-3.0	VFSL	VM	Lac		Silty
		3.0-4.1	VFSL	Sat	Lac		Silty, free water, VFSL sand lenses
		4.1-4.6	SiCL	M	Lac		Stiff, med plastic, olive brown
		4.6-5.0	VFSCL	VM	Lac		Soft, low plastic, olive brown
		5.0-6.2	SiCL	VM	Lac		Firm, low plastic, olive brown
							,
AM4-19	0314411	0-1.0	SiCL	М	Lac		
	5511281	1.0-2.7	VFSL	М	Lac		
		2.7-4.4	VFSL	Sat	Lac		Soft
		4.4-6.2	C-SC	М	Till		Stiff, low plastic, trace gravel
	l	I	I	I		I	I I

Legend: L C S

Loam Clay Sand

С

Gr.	Gravel
Si	Silt
F	Fine (sand)
VF	Very Fine (sand)

Eg. VFSCL = Very Fine Sandy Clay Loam

Untitled Map

Write a description for your map.

AO: This plan was provided as part of the Chilako Drilling Services soil report and shows the location of the test holes which were drilled. The date the photograph is unknown

9AM2-19



%M3-19

9AM4-19

Google Earth

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Page 36 of 100

80 m

N

Photographs provided by Arie Muilwijk showing roller compacted concrete

construction Uncovered / Open pens







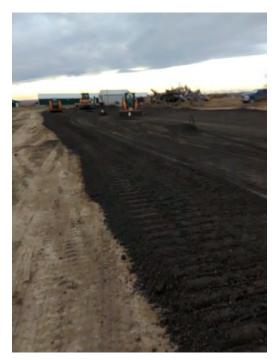








Covered pens











6 November 2020

Wood File: BX30653



3102 – 12 Avenue North Lethbridge, Alberta T1H 5V1 www.woodplc.com

Arie & Willemiek Muilwijk P.O. Box 1628 Fort Macleod, AB TOL 020

Attention: Arie Muilwijk

Re: Compliance Report – Roller Compacted Concrete for Calf Shelter, Calf/Feeder Pens NE-10-009-27-W4M, near Fort Macleod, Alberta

As requested, Wood Environment & Infrastructure Solutions (Wood) has provided engineering support services in conjunction with the recently constructed calf shelter and feeder pens at the above-captioned site. It is understood that the NRBC permitting for this expansion was not quite finalized at the time of construction of the subject shelter and pens, and in the time since construction, several issues have been raised by the NRCB which have to this point encumbered the permitting of the facility. The purpose of this letter is to provide an engineering basis for the design of the shelter and pen base relative to the Agricultural Operation Practices Act, AB Reg. 267/2001 (hereinafter referred to as "AOPA"), to support NRCB permitting of the new facility.

In general, the subject floor of the shelter and base of three pens were constructed using Roller Compacted Concrete (RCC). The RCC mat was constructed with a minimum targeted thickness of 150 mm, and the nominal targeted compressive strength of the concrete was 25 MPa. The RCC was placed in November, 2019.

Construction Review of the RCC Mat

The calf shelter RCC mat encompasses an area of about 15 m wide by 80 m long, and is located directly east of the residence and north of the barns (*see Figure 1*). The new feedlot pens encompass an area of about 37 m wide by 97 m long, and are located just southeast of the calf shelter building (see Figure 1). At the time of Wood's field review, the catch basin had been formed, but the liner was not installed. The catch basin excavation measured roughly 20 m wide by 30 m long by 1.8 m deep, with side slopes of approximately 3 horizontal to 1 vertical (i.e., 3H:1V).

To assess the RCC mat, Wood reviewed records of construction, the concrete mix, and carried out testing and field review of the completed RCC mat. Construction of the RCC mat was carried out by Subterrain Excavating, who leveled and prepared the subgrade, and placed the RCC. The RCC was supplied by Prairie Stone Concrete, who had set up their plant at the White Lake Colony gravel pit, located along the Spring Point Road (Hwy 785), about 5 km from the site.

The site review by Wood was carried out on June 9, 2020, and included coring, non-destructive compressive strength testing, and a visual review of both mats to the extent possible. The following comments, observations, and test results by Wood relative to the recently placed RCC mat are provided as follows:





- 1. The sizes and locations of the calf shelter, pens, and catch basin are generally consistent with the details provided in the NRCB Permit Application (LA19036).
- 2. Photographs provided depicted the subgrade prior to placement of the RCC and showed that the subgrade had been levelled and compacted prior to RCC placement.
- 3. The RCC was placed by Subterrain Excavating using GPS based survey-controlled equipment to provide a uniform placement thickness of RCC and positive sloping of the pens. Based on coring of several locations in the RCC, the thickness of RCC ranged between 155 mm and 205 mm, with an average thickness of 173 mm for eight cores *(see Concrete Core Report, attached)*. The approximate core locations are illustrated on *Figure 1*, attached.
- 4. Photographs provided depicted the RCC being compacted around existing fence posts, waterers, and bunk aprons, using a walk-behind plate compactor, while a large vibrating ride-on compactor was used to compact the majority of the RCC.
- 5. Further photographs provided depicted a layer of straw over the RCC following placement to promote curing of the RCC and to provide crack control related to early-stage curing of the RCC.
- 6. Laboratory density testing was carried out on core samples recovered from the RCC mat, and indicated in-place densities ranging between 2,395 kg/m³ and 2,420 kg/m³, generally representing optimal compaction of the RCC mix, with densities ranging between 99 percent and 101 percent of the target mix density of 2,400 kg/m³ (see Concrete Core Report, attached).
- 7. During Wood's June 9, 2020 site visit, a Schmidt hammer was utilized to estimate the compressive strength of the RCC. The results of the rebound testing indicated compressive strengths of the RCC ranging between about 25 MPa and 40 MPa.
- 8. At the time of Wood's site review, the catch basin had also been roughly formed, and dimensions were found to be in general accordance with those provided in the application for permit. No accumulation of water or evidence of groundwater was observed in the catch basin excavation. Some accumulation of sand and silt was observed, which would require removal prior to placement of a liner. It is understood that an HDPE liner is proposed for this catch basin.

Roller Compacted Concrete (RCC) as a Liner

The use of RCC is gaining widespread popularity and acceptance among producers in the confined feeding industry in Southern Alberta. Since 2018, the local Lethbridge NRCB office has also permitted the construction of at least one feedlot expansion¹ with RCC as the pen base, with consideration of the RCC as a liner material meeting the requirements of the AOPA. Given the questions surrounding the use of RCC as a liner satisfying the requirements of AOPA, most of the local RCC pen base construction has encompassed the rehabilitation of older 'grandfathered' confined feeding operations or existing permitted facilities as an alternative to the ongoing requirement for imported clay to reconstruct pen bases following manure removal. Wood provided engineering support to one of the first projects

¹ NRCB permit: LA18053B

Arie & Willemiek Muilwijk Compliance Report – Roller Compacted Concrete for Calf Shelter, Calf/Feeder Pens NE-10-009-27-W4M, near Fort Macleod, AB 6 November 2020 Page 3



associated with the recent onslaught of RCC use as a pen base more than ten years ago. That first project, as well as the associated widespread use of RCC that has developed in the more recent few years, has consistently demonstrated that RCC is robust and performs very well for many years both in terms of animal health and performance of the pen bases during all cycles of pen cleaning activities and animal occupation.

While the NRCB has released a document entitled "Non-Engineered Concrete Liners for Manure Collection and Storage Areas" (dated June 2015), this provides guidance for the use of conventional reinforced plastic concrete, and is not directly applicable to the use of RCC as a liner material. At this time neither Alberta Agriculture nor the NRCB have released an official guidance document to support the use of RCC as a liner material for solid manure storage. Accordingly, this letter is prepared to satisfy the intent of AOPA Section 9(6), which indicates: "The liner of a manure storage facility and of a manure collection area, if constructed of compacted soil or constructed of concrete, steel, <u>or other synthetic or manufactured</u> <u>materials</u>, must provide equal or greater protection than that provided by compacted soil (c)0.5m in depth with a hydraulic conductivity of not more than 5×10^{-7} centimetres per second for a solid manure storage or solid manure collection area.", by providing engineering rational to support RCC as a liner which satisfies AOPA Section 9(6)c.

The use of concrete as a liner in past years, even in the case of completely unreinforced concrete, has demonstrated significant longevity, *and generally performs better than compacted soil, HDPE, or steel.* An important advantage of concrete, whether conventional concrete or RCC, is the level to which positive drainage can be maintained within the pen areas as compared to clay-lined pens. Particularly, RCC pens are generally characterized by much less ponding than for clay pens, and where water is efficiently shed off the mat rather than allowed to pond in the pen, the net result is that the volume of surface water available to permeate through the pen base is much less than for RCC pens. The more efficient shedding of water from the pen area also helps to mitigate the freeze/thaw effects on the soil subgrade or compacted clay liner, which is a major contributor to soft clay pen base conditions during spring months.

The readily available publication "*Design and Control of Concrete Mixtures*" by the Cement Association of Canada provides a good discourse on volume changes related to concrete. Cracking of concrete can be primarily attributed to slight volume changes in the concrete, particularly in conjunction with tension stresses that develop because of shrinkage. This volume change (or shrinkage) occurs for a variety of reasons. In early concrete stages, chemical shrinkage occurs in conjunction with the reduction in volume of solids and liquids in paste resulting from cement hydration. Autogenous shrinkage occurs at a macroscopic level where there is visible dimensional change of the cement paste resulting from hydration. Subsidence occurs in the form of vertical shrinkage of fresh concrete as bleed water rises to the surface. And plastic shrinkage occurs in the case that rapid evaporation of moisture from the surface of the concrete exceeds the bleeding rate. Following hardening of the concrete, volume changes occur as a result of moisture changes (with shrinkage occurring as a result of moisture loss and expansion during moisture gain), and as a result of temperature changes (with contraction occurring during cold weather, and expansion occurring during warmer weather.



The level of early age volume changes related to roller compacted concrete is generally considered to be *somewhat lower* than for conventional (plastic concrete) due to the typical lower water content and watercement ratio of the concrete, the general absence of bleed water, and the effect of compacting the concrete matrix into place during placement. However, based on Wood's experience, the volume changes of the roller compacted concrete resulting from moisture changes or thermal expansion/contraction appear to be consistent with conventional concrete. Assuming a coefficient of thermal expansion of 8 x 10⁻⁶ per degree Celsius for concrete using sand and gravel, the calculated linear change of a concrete pad associated with a temperature variation between -30 °C and +30°C would be about 5 mm per 10 m length of concrete. Assuming a similar reduction in volume during early age curing, and an additional 10 mm of further propagation of these cracks after a series of seasonal cycles, it would be reasonable to assume typical long-term potential crack propagation to 20 mm per 10 m length of RCC at the subject site. This is generally consistent with Wood's observations of older RCC mats, though it is noted that after one year no readily observable cracking was noted in the RCC mats at the subject Muilwijk operation.

Invariably, the cracks in the RCC mat become infilled with a combination of bedding material, manure, and soil. While Wood does not know of any studies specifically measuring permeability through infilled cracks of a manure storage pad, some excellent work has been done to measure permeability through the black interface and gleyed zone occurring in conjunction with moderately coarse and moderately fine textured soils in feedlot pen surfaces in Southern Alberta². The intent (in part) of the referenced study was to investigate this black interface layer between the manure pack and underlying stained soils to assess suitability of this material relative to protection of groundwater. The results of the study indicated permeability through this black interface zone or (in some cases a gleyed layer) would not directly satisfy the stated AOPA requirements for groundwater protection, the localized higher permeability through these narrow interface zones (i.e., infilled cracks) can be considered in conjunction with the broader relatively impermeable RCC (or concrete) matrix.

Permeability through RCC and typical hardened concrete is widely documented, and generally below 1×10^{-9} cm/sec. Considering a 10 m by 10 m section of RCC mat containing one 20 mm wide crack in both directions (the cracked area having an assumed permeability of 1×10^{-4} cm/sec), and a conservative estimate of 1×10^{-9} cm/sec for RCC, the average calculated permeability through the 150 mm thick RCC mat would be 9.0×10^{-8} cm/sec. This represents the equivalent of approximately 0.8 m of compacted soil having a hydraulic conductivity of 5×10^{-7} cm/sec, which is more than the minimum 0.5 m of compacted soil having a hydraulic conductivity of 5×10^{-7} cm/sec indicated by Section 9(6)c for solid manure storage or solid manure collection. It is noted that both the hydraulic conductivity of the RCC and interface zone (cracks) indicated above would be considered conservative estimates of hydraulic conductivity.

² Jim J Miller, Tony Curtis, Francis J. Larney, Tim A. McAllister, and Barry M. Olson: *"Physical and Chemical Properties of Feedlot Pen Surfaces Located on Moderately Coarse- and Moderately Fine-Textured Soils in Southern Alberta"* Journal of Environmental Quality, Volume 37, July-August 2008.

³ Note: Miller et al reports field-saturated hydraulic conductivity, K_{fs} , of 4.37 to 92.9 x 10⁻⁷ m s⁻¹ for pen base soils at the three study sites.

Arie & Willemiek Muilwijk Compliance Report – Roller Compacted Concrete for Calf Shelter, Calf/Feeder Pens NE-10-009-27-W4M, near Fort Macleod, AB 6 November 2020 Page 5

wood.

Closing Comment

In general, the review of the RCC associated with the subject calf shelter and pens indicated that construction of the RCC mat was consistent with good construction practice. Further, the results of density and compressive strength testing of the finished mat indicate that the RCC is competent and suitable for its intended purpose.

Finally, as demonstrated in the discussion provided above it is Wood's opinion that the Roller Compacted Concrete (including with the consideration of potential cracking as outlined herein) satisfies the requirements for liner material indicated in Section 9(6)c of the AOPA.

This report has been prepared for the exclusive use of Arie & Willemiek Muilwijk for the specific application to the development described in this report, and may be used by the NRCB specifically to support the permit application by the Muilwijk's for the subject calf shelter and calf/feeder pens as described herein. Any use that a third party makes of this report, or any reliance or decisions based on this report are the sole responsibility of those parties. This report has been prepared in accordance with generally accepted soil and materials engineering practices. No other warranty, express or implied, is made.

We trust this satisfies your present requirements. If you have questions or require further information or clarification, please do not hesitate to contact the undersigned.

Respectfully submitted,

Wood Environment and Infrastructure Solutions, A Division of Wood Canada Limited

=NOIN lormb.

John Lobbezoo, P.Eng. @@@ Associate Engineer, Geotechnical Lethbridge Geotechnical & Materials Testing Lead

Attachments: Figure 1 – Site Plan Concrete Core Report *Reviewed by:* Cody Metheral, P.Eng. Linkage Ag Solutions

Adam Johnson, C.E.T. Field & Laboratory Services Manager

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PERMIT NUN The Association	BER: P-04546 on of Professional oscientists of Alberta

i.



Site Plan New Pen/Calf Shelter Construction Arie & Willemiek Muilwijk NE-10-009-27-W4M Wood File: BX30653

Page 45 of 100

Legend: *A

RCC Core Location

CONCRETE CORE REPORT

CCILC CERTIFIED CONCRETE TESTING LABORATORY



Project No.: BX30653

Wood Environment & Infrastructure Solutions a Division of Wood Canada Limited Lethbridge Laboratory

To: Arie & Willemiek Muilwijk Box 1628 Fort Macleod, AB TOL 0Z0

Attention: Arie Muilwijk

Project: Material Testing Services

SPECIMEN NUMBER	DATE TESTED	RAW SPECIMEN LENGTH (mm)	SPECIMEN DENSITY (kg/m³)	PERCENT OF TARGET DENSITY (%)	CORE LOCATION
А	10-Jun-20	168	2413	100.5%	Calf Shelter (see drawing)
в	10-Jun-20	183	2401	100.0%	Calf Shelter (see drawing)
с	10-Jun-20	205	2420	100.8%	Calf Shelter (see drawing)
D	10-Jun-20	170	2405	100.2%	Calf Shelter (see drawing)
Е	10-Jun-20	155	2395	99.8%	North Pen (see drawing)
E	10-Jun-20	162	2399	100.0%	Centre Pen (see drawing)
G	10-Jun-20	173	2404	100.2%	South Pen (see drawing)
н	10-Jun-20	169	2415	100.6%	South Pen (see drawing)
	Average	173.1	2406.5		
ARGET DE AGGREGAT ADMIXTURI SUPPLIER MIX NO.	'E SIZE ES	@ - 1 2400 k	Ира Days (g/m ³ nm		Page 46 of 10
			out by We 2, <u>Client (</u> related to	otherwise noted, all asp bod personnel conform t <u>Cast Cylinders</u> : Various client cast cylinders, if a he in conformance to CS	o CSA CAN A23.2. a Division of Wood Canada Limited testing aspects opplicable,

AO: Groundwater and Uppermost Groundwater Resource Report prepared as part of the ERST scoring for the CFO facilities

LA19036 Site Information Form Supporting Information Groundwater Resource and Uppermost Groundwater Resource (UGR) – NE 10-9-27 W4 December 3, 2020

What groundwater resources exist at this site?

The groundwater resource definition (Appendix A) (i) "means an aquifer below the site of a confined feeding operation or a manure storage facility that is being used as a water supply for the purposes of domestic use".

Part A of the groundwater resources definition (ii) discusses an aquifer with a sustained yield of 0.76 L/minute or more and a total dissolved solids (TDS) concentration of 4000 mg/L or less.

Existing water well's groundwater resource

Water well id 115735 is the only current water well within 400m of all facilities at this site. It was drilled in 1982 to a depth of 29.0m, with perforations from 24.4m to 29.0m (Appendix B). Formations logged were brown till (surface to 12.2m), underlain by blue clay (12.2m to 22.9m), and underlain by hard shale and gravel (22.9m to 29.0m). The static water level was identified as 18.9m. None of the formations are identified as water bearing in the formation log column. As the well was completed (and perforated into) the hard shale and gravel formation (and only that formation), the hard shale and gravel will be considered a water bearing aquifer. The formation is under sufficient confinement by the blue clay layer above that the water level rose to 18.9m, 4m above the top of the hard shale and gravel. The water level did not rise as high as the brown till, suggesting that the brown till and hard shale and gravel formations are hydrogeologically separate. Proposed well use is "Domestic & Stock". Because it is an aquifer for domestic use, the hard shale and gravel identified in well id 115735 is a groundwater resource.

Are there other groundwater resources at site?

The lithology for water well id 115735 does not indicate a shallower aquifer than the hard shale and gravel groundwater resource from 22.9m to 29.0m.

Water well id 115734 is a 1980 chemistry report from a well on site (Appendix B). The method of drilling was "Hand Dug", proposed well use was "Domestic", and the total depth of the well is identified as 4.6m. Lithology is not listed (as was very common for chemistry reports). This is clearly a different water well than id 115735, which was drilled in 1982. At some point in the past, well id 115734 was "being used as a water supply for the purposes of domestic use", so it would have been completed into an aquifer. However, well id 115734 is no longer in use, so the aquifer it was completed into is no longer in use at this site.

The (i) definition of groundwater resource is "an aquifer below the site of a confined feeding operation ... *that is being used* as a water supply for the purposes of domestic use." (emphasis added) I note that this definition is specific that an aquifer must be below a confined feeding operation to be considered a groundwater resource, but the definition is not specific about the location of the domestic use of the aquifer. In other words, an aquifer that existed below a confined feeding operation (CFO) (but not used by the CFO) yet was used by a neighbouring residence for domestic use would be considered a groundwater resource and require a liner or layer between manure facilities and the groundwater resource below the CFO site.

Within what distance should other domestic users of groundwater be looked for?

The Environmental Risk Screening Tool, version 1.2, September 2011, page 10, (Appendix C) states:

"The depth to the UGR should be determined using site-specific information when available (e.g. borehole logs or monitoring well completion information in geotechnical or hydrogeological reports).

If the site-specific geological information shows that there may be a shallower aquifer located above the aquifer used on site, then the water well drillers logs from wells located within 1.6km (1 mile) of the facilities property boundary (quarter section) need to be reviewed.

The uppermost aquifer within 1.6km (1 mile) currently in use must be correlated to the site specific information to call this identified uppermost aguifer on site the UGR."

What information was found?

A reconnaissance report from Alberta Environment's Groundwater Information Database for the NE 10-9-27 W4 plus 1.6km in all directions yielded 27 results. (Appendix D) The depth column was reviewed. All wells reports with a well depth equal to or less than 20 feet (including 0 feet) were reviewed with any associated chemistry results (Appendix E), and are summarized in Table 1.

Well id	Land	Depth	Well id report	Total	Year	Other
	Location	(feet/	type	Dissolved	Report	
	(of 9-27W4)	metres)	• •	Solids (mg/L)	Received	
115717	NE 3	5.0/1.5	Chemistry	446	1978	
115719	NE 3	20.0/6.1	Chemistry	489	1980	1985 – owner
						reports well yield
						has decreased ²
155266	NE 3	0.0 ¹	Chemistry	188	1990	
2093787	SE 10	13.0/4.0	Well	No chemistry	1985	Prior to 1984,
			Inventory	information		yielded 10 gpm
			(Drilled			1985, yielded 5
			1978/11/05)			gpm
						1985 – well
						service, 24" of
						gravel removed
						from well bottom ²
115734	NE 10	15.0/4.6	Chemistry	461	1980	
244439	SE 14	0.0 ¹	Chemistry	268	1987	
115750	NW 14	13.0/4.0	Test Hole, 2	No water	1986	Lithology:
			inch plastic	levels or		0-2', Gravel
			casing	chemistry		2'-7', Silty clay
			installed	information		7'-11', Medium
						grained sand
						11'-13', Silty clay

Table 1. Summary of Well ids and Associated Chemistry results

¹A well depth of 0.0 is assumed to be unknown

²Emergency Groundwater Testing Program

Working up from the bottom of Table 1, well id 115750 will not be further assessed because it has no evidence of water presence.

Well id 244429 will not be further assessed because it could be a subsequent chemistry that was done on well id 115746 (1985 chemistry report on a well reported to be 200 feet deep).

Well id 115734 is the shallow well on site, discussed above.

All water well ids for SE 10-9-27W4 were searched, two were found. One is a well inventory (well id 2093787) drilled in 1978. The other well (id 115732) was drilled in 1985. Both wells are listed as having the same owner. The 1978 water well report indicates it's use was domestic and stock, a well depth of 13.0 feet, and a 10 gpm yield (prior to 1984), reduced to a 5 gpm yield (1985). This well was serviced in 1985 and 24" of gravel was removed from the well. The well depth for the 1978 well is similar to the water depth on NE 10. The flow rates of 10 and 5 gpm are greater than the 0.76 L/min minimum in the groundwater resource definition. There is no chemistry information attached to well id 2093787.

All water well ids for NE 3-9-27W4 were searched; four were found. Three are chemistries (well ids 115717, 115719 and 155266), and one is an Alberta Environment test hole that was not completed as a water well. There is no record of a water well being drilled at NE 3. The well depth reported for each of the three water wells is 20.0 feet (or less), similar to the water depth on NE 10. Each of the TDS results for NE 3 are <500 mg/L, below the 4000 mg/L in the groundwater resource definition.

Rural domestic water use changes over time

The Environmental Risk Screening Tool, version 1.2, September 2011, page 9, (Appendix C) discusses Alberta Environment well records from the early 1900s to the Second World War, and that wells that provided enough water pre-Second World War for domestic purposes may not provide sufficient water for residential use today. All five of these shallow well reports for NE10, SE10, and NE3 are from 1978 or later. This is the "modern" era of required yield of water for rural domestic purposes – the era of electricity, running water, dishwashers, washing machines, indoor toilets, showers, etc. Because of the decades between the Second World War and the earliest of these shallow well reports in 1978, none of these shallow wells can be discounted as having insufficient supply due to changes in domestic rural household water use over time.

Other site information regarding groundwater

Four boreholes were advanced on site on August 9, 2019 from surface to depths of 6.2m. Borehole logs and their location were provided (Appendix F), but without an accompanying report. All four boreholes indicate a saturated zone, with a top ranging from 2.7m to 3.6m below surface, and a bottom ranging from 4.1m to 5.6m below surface (Table 2).

	Hole #	Depth ¹	Texture	Moisture ²	Remarks related to saturation
	AM1-19	3.5-5.1	VFSL ³	VM-Sat	Slough @ 3.3m
ĺ	AM2-19	3.6-5.6	VFSL	Sat	Soft, olive brown, silty, free water;
					slough @ 3.9m
	AM3-19	3.0-4.1	VFSL	Sat	Silty, free water, VFSL sand lenses
	AM4-19	2.7-4.4	VFSL	Sat	

Table 2. Borehole information for Arie Muilwijk (saturated zones)

¹All depths assumed to be in metres.

²VM assumed to be Very Moist, Sat assumed to be Saturated

³VFSL is Very Fine Sandy Loam (as per legend provided)

All four boreholes indicate a saturated zone (a water table) shallower than the hard shale and gravel formation. The presence of this water table across all four boreholes and the similar depth as well id 115734 are supporting information that the aquifer used in water well id 115734 is laterally extensive, at minimum within the area of the boreholes on site.

So, after reviewing all this information, are there other groundwater resources below the site?

Yes. There is enough information that a shallow aquifer extends from NE10, south onto SE10 and further south onto NE3. It may still be in use on SE10 via a water well, and is most likely still in use on NE3 via a water well. All chemistry and yield data from the five shallow wells on these three quarter sections meet (ii) of the groundwater resource definition.

The aquifer that well id 115734 was completed into, further detailed in depth and extent by the four onsite boreholes, is a groundwater resource below the site.

What is the Uppermost Groundwater Resource?

The uppermost groundwater resource at NE10-9-27W4 is the shallow aquifer that well id 115734 was completed into. On site, the depth to the top of the UGR ranges from 2.7m to 3.6m below grade, based on saturated very fine sandy loam zones indicated in the four borehole logs.

The shallowest top of UGR depth will be entered on Site Information Forms for all facilities because that is a reasonably conservative assumption for screening level assessment:

Reference: borehole AM4-19 Predominant geology: very fine sandy loam [2.7m to 4.4m] Depth to UGR from ground level: 2.7m Subsoil Texture: Coarse

A subsoil texture of coarse was chosen for the UGR based on the ERST's Reference Materials (Appendix G). "Coarse" includes Clean Sand (fine), silty sand, and some silt, so I determined coarse was the most appropriate category for very fine sandy loam. In addition, well id 2093787 indicates a pre-1984 flow rate of 10gpm from this zone.

Scott Cunningham Scott Cunningham, P.Eng, P.Ag.

December 3, 2020

Page 4 of 5

Page 50 of 100

Appendix A – Groundwater Resource definition

- Appendix B Site Water Well Reports
- Appendix C Environmental Risk Screening Tool (pages 9 and 10)
- Appendix D Water Well Reconnaissance Report and Map
- Appendix E Water Well Reports within 1.6km of the Site
- Appendix F Site Borehole Logs and Locations
- Appendix G Environmental Risk Screening Tool (estimating subsoil texture)

Appendix A

Groundwater Resource definition

Standards and Administration Regulation AR267/2001

- (vi) a storm drainage system as defined in the *Environmental Protection and Enhancement Act*, and
- (vii) a temporary stream on private land controlled by the owner or operator that has no outflow going beyond the private land directly to a drainage canal, reservoir, river, permanent stream or creek, lake or potable water source that is being used for human or livestock consumption;
- (e) repealed AR 85/2004 s1;
- (f) repealed AR 215/2006 s2;
- (g) "freeboard" means the vertical distance between the full storage level of a structure and the upper edge of the structure;
- (g.1) "groundwater resource" means an aquifer below the site of a confined feeding operation or a manure storage facility
 - (i) that is being used as a water supply for the purposes of domestic use, or
 - (ii) if no aquifer referred to in subclause (i) exists,
 - (A) an aquifer that has a sustained yield of 0.76 litres per minute or more and a total dissolved solids concentration of 4000 milligrams per litre or less as determined by well records, well drilling logs, hydrogeological maps, hydrogeological reports or other evidence satisfactory to an approval officer or the Board, and
 - (B) if there is more than one aquifer that meets the requirements of paragraph (A), the aquifer that an approval officer or the Board considers to be the best suited for development as a water supply for the purposes of domestic use;
 - (h) "liner" means, with respect to a manure storage facility or manure collection area, a layer constructed out of natural or manufactured materials that restricts the migration of the contents of the manure storage facility or manure collection area;
 - (i) "liquid manure" means manure that is in a predominantly liquid state or manure to which water has been added;

Appendix B

Site Water Well Reports

NE10-9-27W4



The driller supplies the data contained in this report. The Province disclaims responsibility for its

View in Metric Export to Excel

115735

GoA Well Tag No.

GIC Well ID

Drilling Company Well ID accuracy. The information on this report will be retained in a public database GOWN ID Date Report Received 1982/12/14 Well Identification and Location Measurement in Imperial Owner Name Address Postal Code Town Province Country HAWTHORNE, WAYNE P.O. BOX 1251 CLARESHOLM SEC TWP 1/4 or LSD RGE W of MER Block Additional Description Location Lot Plan 15 10 9 27 4 GPS Coordinates in Decimal Degrees (NAD 83) Measured from Boundary of Elevation Latitude 49.725817 Longitude -113.578252 ft ft from How Location Obtained How Elevation Obtained ft from Map Not Obtained **Drilling Information** Type of Work Method of Drilling Rotarv New Well **Proposed Well Use** Domestic & Stock Formation Log Measurement in Imperial Yield Test Summary Measurement in Imperial Recommended Pump Rate 0.00 igpm Water Depth from Lithology Description ground level (ft) Water Removal Rate (igpm) Static Water Level (ft) Bearing Test Date 40.00 Brown Till 1982/09/20 16.00 62.00 75.00 Blue Clay Well Completion Measurement in Imperial Total Depth Drilled Finished Well Depth Start Date End Date 95.00 Hard Shale & Gravel 95.00 ft 1982/09/20 1982/09/20 **Borehole** Diameter (in) From (ft) To (ft) 0.00 0.00 95.00 Surface Casing (if applicable) Well Casing/Liner Steel Steel Size OD : 7.00 in Size OD : 4.50 in 0.000 in 0.188 in Wall Thickness : Wall Thickness : Bottom at : 6.00 ft Top at : 0.00 ft Bottom at : 95.00 ft Perforations Slot Length Hole or Slot Diameter or To (ft) From (ft) Slot Width(in) Interval(in) (in) 80.00 95.00 0.188 5.00 Perforated by Torch Annular Seal Driven Placed from 0.00 ft to 6.00 ft Amount Other Seals At (ft) Type Screen Type Size OD : 0.00 in Slot Size (in) From (ft) To (ft) Attachment Top Fittings Bottom Fittings Pack Type Grain Size Amount Contractor Certification Name of Journeyman responsible for drilling/construction of well Certification No UNKNOWN NA DRILLER 1

Company Name HENNING DRILLING LTD. Copy of Well report provided to owner Date approval holder signed



The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

GoA Well Tag No.

Drilling Company Well ID

GIC Well ID

115735

View in Metric Export to Excel

GOWN ID	····, · · · · · ·				Date Report Receit	ved 1982/12/14
Well Identification and Location						Measurement in Imperia
<i>Owner Name</i> HAWTHORNE, WAYNE	Address P.O. BOX 1251 CLAI	RESHOLM	Town	Province	e Country	Postal Code
Location1/4 or LSDSEC1510	<i>TWP RGE</i> 9 27	4			onal Description	
Measured from Boundary of ft from ft from			in Decimal Degrees 5817 Longitud ained		Elevation How Elevation Ob Not Obtained	
Additional Information						Measurement in Imperia
Distance From Top of Casing to Gro Is Artesian Flow Rate			Is Flow Control	Installed Describe		
Recommended Pump Rate Recommended Pump Intake Depth		0.00 igpm	Pump Installed Yes	3	Depth	ft H.P5 Rating)
Did you Encounter Saline Water (Additional Comments on Well DRILLER REPORTS WATER IS SC	Gas		ft		og Taken to ESRD	
Yield Test					Ground Level	Measurement in Imperia
Test Date Start Tin 1982/09/20 12:00 AM		ic Water Level 62.00 ft	Pumpir		Elapsed Time Minutes:Sec	Recovery (ft)
Method of Water Removal Type <u>Bailer</u> Removal Rate Depth Withdrawn From If water removal period was < 2 hou	62.00 ft					
Water Diverted for Drilling						
Water Source	Am	nount Taken ig		Divers	ion Date & Time	

Contractor Certification

Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER

Company Name HENNING DRILLING LTD.

Certification No 1

Copy of Well report provided to owner Date approval holder signed



The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

View in Metric Export to Excel 115734 GoA Well Tag No.

Drilling Company Well ID

GIC Well ID

GOWN ID		•				Date Report Received	d 1980/01/17
Well Identification and Location							leasurement in Imperial
<i>Owner Name</i> VAN WAARDHUIZEN, PETER	Address		Town		Province	Country	Postal Code
	P.O. BOX 73 FT N		1 = (Dia dia Dia			
Location 1/4 or LSD SEC NE 10	TWP RGE 9 27	W of MER L 4	Lot	Block Plai	n Addillo	nal Description	
Measured from Boundary of ft from		GPS Coordinates Latitude 49.72 How Location Ob	24009	al Degrees (NA) Longitude _1	· · · · · · · · · · · · · · · · · · ·	Elevation <u>32</u> How Elevation Obtai	225.00 ft
ft from		Мар	Stanloa			Estimated	in ou
					_		
Drilling Information							
<i>Method of Drilling</i> Hand Dug		Type of Work Chemistry					
Proposed Well Use Domestic							
Formation Log	М	easurement in Imperi		ield Test Sum			leasurement in Imperial
Depth from ground level (ft) Bearing	ogy Description		R	Recommended I Test Date	Pump Rate Water Removal		Static Water Level (ft)
				Vell Completic		N I Depth Start Date	Aeasurement in Imperial End Date
				5.00 ft			
			В	Borehole			
				Diameter (0.00	(in)	From (ft) 0.00	To (ft) 15.00
			S		(if applicable)	Well Casing/L	
				_		, i i i i i i i i i i i i i i i i i i i	
					0.00 in		
				Wall Thickness Bottom at			ss : <u>0.000 in</u> at : 0.00 ft
				Dottonnat	<u> </u>	Bottom	
			P	Perforations	Diamete	er or Slot Length	Hole or Slot
				From (ft) T	o (ft) Slot Wid		Interval(in)
			Р	Perforated by			
			A	nnular Seal			
				Placed from	0.00 ft	to 0.00 ft	
			0	Amount			
					Туре		At (ft)
			3	Screen Type	0.00 in		
					:)	To (ft)	Slot Size (in)
				Attachman	4		
				Attachmen Top Fittings	s	Bottom Fitting	gs
			P	Pack			
				Туре		Grain Size	
				Amount			
Contractor Certification							
Name of Journeyman responsible fo UNKNOWN NA DRILLER	or drilling/construction	of well		Certifi 1	ication No		
Company Name UNKNOWN DRILLER				Сору	of Well report pro	vided to owner Date	e approval holder signed



View in Metric Export to Excel

115734

GIC Well ID

Diversion Date & Time

GoA Well Tag No. The driller supplies the data contained in this report. The Province disclaims responsibility for its Drilling Company Well ID accuracy. The information on this report will be retained in a public database GOWN ID Date Report Received 1980/01/17 Well Identification and Location Measurement in Imperial Owner Name Address Town Postal Code Province Country VAN WAARDHUIZEN, PETER P.O. BOX 73 FT MACLEOD TWP RGE W of MER Block 1/4 or LSD SEC Plan Additional Description Location Lot NE 10 9 27 4 GPS Coordinates in Decimal Degrees (NAD 83) Measured from Boundary of Elevation 3225.00 ft Latitude 49.724009 Longitude -113.575461 ft from How Location Obtained How Elevation Obtained ft from Мар Estimated Additional Information Measurement in Imperial Distance From Top of Casing to Ground Level in Is Artesian Flow Is Flow Control Installed Rate Describe iapm Recommended Pump Rate igpm Pump Installed Depth ft Recommended Pump Intake Depth (From TOC) ft Make H.P. Туре Model (Output Rating) Did you Encounter Saline Water (>4000 ppm TDS) Depth ft Well Disinfected Upon Completion Depth ft Geophysical Log Taken Gas Submitted to ESRD Sample Collected for Potability Submitted to ESRD Yes Additional Comments on Well Yield Test Taken From Ground Level Measurement in Imperial

Amount Taken

ig

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed

Water Source

Appendix C

Environmental Risk Screening Tool

Companion document, pages 9 and 10

If the 'Type of Work' on a water well drillers log is indicated as chemistry, this may be a water sample that was taken from an existing well and not an indication of another well on the quarter section. However, if no other well logs exist for the quarter section, it could be an indication that there is an existing well that was never entered into Alberta Environment's system.

Alberta Environment's Information System includes well inventory and federal well survey logs reported approximately from the early 1900s to the Second World War. Generally, these well reports include much less information on depth, completion and water volumes than more recent well reports. Many of these wells are shallow, and were either hand dug or drilled using horse powered drilling. These wells generally provided suitable volumes of water for pre World War II residential use of washing and cooking but may not meet today's UGR volume requirements for residential water use. If a well inventory or federal well survey water well is still in use, then it should be entered on the site information form. If a well inventory or federal well survey water well is no longer in use at a site, it should be considered a decommissioned well (whether documented or not) and should not be included on the site information form.

Indicate the well identification number from the water well drilling log in Alberta Environment's Information System. If a well log was not filed with Alberta Environment, assign a name to the well on the log in the file and indicate same name on the table.

- Distance to well(s) Note the distance to any water wells within 400 metres of a manure storage facility or catch basin.
- Well Sealing Method Indicate how the water wells located within 400 m of the facility are constructed and sealed (e.g. driven seal). This information can be obtained from well completion information in water well drilling logs. If the water well drilling log does not contain any well sealing details, then indicate that well sealing method is unknown. Wells where the annulus is sealed with bentonite or cement are considered the standard or baseline.
- Depth to top of open interval The depth to the top of the open interval (e.g. open hole, slotted casing or well screens) can be determined by using well completion information. The depth to the top of the open interval is the distance from ground surface to the top of the open hole, slotted casing or well screens.

If the bottom of the seal in a water well is shallower than the top of the screened, slotted or open hole portion of the well, and if the geologic materials between the bottom of the seal and the top of the screened, slotted or open hole portion of the well contribute substantially to well yield, then the depth to the bottom of the seal should be considered the depth to the top of the open interval.

Location of well(s) from the reference point – In ideal situations, water level elevation information from site-specific groundwater monitoring wells completed at approximately the same depth should be used to determine the direction of shallow groundwater flow. In situations where this information is not available, the land surface topography can be a good general indicator of shallow groundwater flow direction, since water table slope often mimics surface topography. Topographical information is readily available from topographical maps (MTS 1:50,000 preferred). If after looking at topography information from maps and from a site visit, you are still uncertain about whether or not a water well is upslope or down slope of a facility, choose the most conservative approach when scoring the facility, which is "unknown".

Environmental risk screening tool for manure facilities at confined feeding operations

Note the position of the water well(s) with reference to the facilities being assessed as follows (choose the closest facility requiring scoring for the purposes of the site information form):

- Unknown Choose 'Unknown' if it cannot be determined whether or not a water well is conclusively located upslope or downslope from the facility being assessed, or is located cross slope.
- Down slope Well is conclusively located down slope from the facility being assessed.
- Upslope Well is conclusively located upslope from the facility being assessed.
 - There may be situations where a producing water well may be at risk even if it is determined to be upslope of the facility. Pumping of the well results in a cone of depression that could extend beneath the facility and draw contaminated water toward the well. The size of a cone of depression is dependent on many factors including the pumping rate of the well and hydraulic properties of the aquifer. If not choosing 'Unknown', the use of special consideration points is recommended in cases where a pumping well is located upslope but relatively close to the facility.

8. Uppermost Groundwater Resource (UGR)

- Reference(s) for uppermost groundwater resource (UGR) Indicate what sources of information were used to determine the UGR. For example, indicate the well I.D.s of the well logs used (could include information from decommissioned, chemistry and well inventory logs) or information on other boreholes in the area of the facility that were used.
- Depth to UGR The UGR is defined by *AOPA*. The depth to the UGR should be determined using site-specific information when available (e.g. borehole logs or monitoring well completion information in geotechnical or hydrogeological reports).

If the site-specific geological information shows that there may be a shallower aquifer located above the aquifer used on site, then the water well drillers logs from wells located within 1.6 km (1 mile) of the facilities property boundary (quarter section) need to be reviewed. Since the UGR definition within *AOPA* does not specify where the aquifer underlying the site must be used as a water supply, it was determined to mean within a reasonable distance from the location of the manure storage. The distance specified for the purposes of the ERST is 1.6 km (1 mile) of the facilities boundary (quarter section). The uppermost aquifer within 1.6 km (1 mile) currently in use must be correlated to the site specific information to call this identified uppermost aquifer on site the UGR.

When site-specific information is not available, the depth to the UGR can be estimated using regional hydrogeology maps and/or information from water well drillers logs from wells located within 1.6 km (1 mile) of the facilities property boundary (quarter section).

- Predominant geology of the UGR Using the most site-specific information available, indicate the predominant geology of the UGR (e.g. sandstone, coal). If the material is very heterogeneous (multiple layers of different geologic materials), then the geologic unit that has the highest hydraulic conductivity should be considered.
- Subsoil Texture of the UGR Subsoil texture refers to the predominant grain size distribution. Using the "Estimating Subsoil Texture" table in Appendix 4, information about the geology of the UGR can be used to estimate the subsoil texture (i.e. fine,

Appendix D

Water Well Reconnaissance Report and Map

NE10-9-27W4 Plus a 1.6km radius

Alberta

Reconnaissance Report

View in Metric Export to Excel

Groundwater Wells

Please click the water Well ID to generate the Water Well Drilling Report.

GIC Well ID	LSD	SEC	тwр	RGE	м	DRILLING COMPANY	DATE COMPLETED	DEPTH (ft)	TYPE OF WORK	USE	СНМ	LT	РТ	WELL OWNER	STATIC LEVEL (ft)	TEST RATE (igpm)	SC_DIA (in)
<u>115714</u>	NW	3	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-16	105.00	New Well	Unknown		6		ALTA ENV #1826E			5.56
<u>115715</u>	11	3	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-17	120.00	Test Hole	Unknown		5		ALTA ENV #1827E			0.00
<u>115716</u>	11	3	9	27	4	HENNING DRILLING LTD.	1984-04-18	101.00	New Well	Domestic & Stock		4		SCHAMP, LOTHER	85.00	9.00	7.00
<u>115717</u>	NE	3	9	27	4	UNKNOWN DRILLER		5.00	Chemistry	Domestic	1			VAN WAARDHUIZEN, PETER			0.00
<u>115718</u>	9	3	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-13	100.00	Test Hole	Unknown		3		ALTA ENV #1824E			0.00
<u>115719</u>	NE	3	9	27	4	UNKNOWN DRILLER		20.00	Chemistry	Domestic	1			SIEBERT, JOHN			
<u>115722</u>	10	4	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-13	115.00	Test Hole	Unknown		6		ALTA ENV #1825E			0.00
<u>115723</u>	NE	4	9	27	4	H&H DRILLING	1989-06-22	110.00	New Well	Domestic		4		BRAUER, MONTY	92.00	10.00	6.63
<u>115732</u>	1	10	9	27	4	VANDRIESTEN WM	1985-08-06	95.00	New Well	Domestic		3		NEELS, GERALD	72.00	18.00	
<u>115733</u>	3	10	9	27	4	VANDRIESTEN WM	1979-04-20	103.00	New Well	Domestic		3		SCHMIDT, NEWTON	80.00	10.00	0.00
<u>115734</u>	NE	10	9	27	4	UNKNOWN DRILLER		15.00	Chemistry	Domestic	1			VAN WAARDHUIZEN, PETER			0.00
<u>115735</u>	15	10	9	27	4	HENNING DRILLING LTD.	1982-09-20	95.00	New Well	Domestic & Stock	1	3		HAWTHORNE, WAYNE	62.00	16.00	7.00
<u>115736</u>	NW	11	9	27	4	ALBERTA ENVIRONMENTAL PROTECTION/TECHNICAL SERVICES DIVISION	1978-07-12	85.00	Test Hole	Unknown		7		ALTA ENV #1821E			0.00
<u>115737</u>	NW	11	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-12	80.00	Test Hole	Unknown				ALTA ENV #1822E			0.00
<u>115738</u>	11	11	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-12	83.00	Test Hole	Unknown				ALTA ENV #1820E			0.00
<u>115746</u>	SE	14	9	27	4	UNKNOWN DRILLER		200.00	Chemistry	Domestic & Stock	1			WALDIE, BRIAN			0.00
<u>115747</u>	SW	14	9	27	4	UNKNOWN DRILLER		150.00	Chemistry	Domestic	<u>1</u>			WALDIE, BRIAN			0.00
<u>115748</u>	3	14	9	27	4	Maughan, Joseph R.	1967-01-01	115.00	Well Inventory	Stock	1						0.00
<u>115749</u>	NW	14	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1978-07-13	80.00	Test Hole	Unknown		5		ALTA ENV #1823E			0.00
<u>115750</u>	NW	14	9	27	4	ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	1986-09-11	13.00	Test Hole	Unknown		4		GROUNDWATER INVEST. #5067-T			0.00

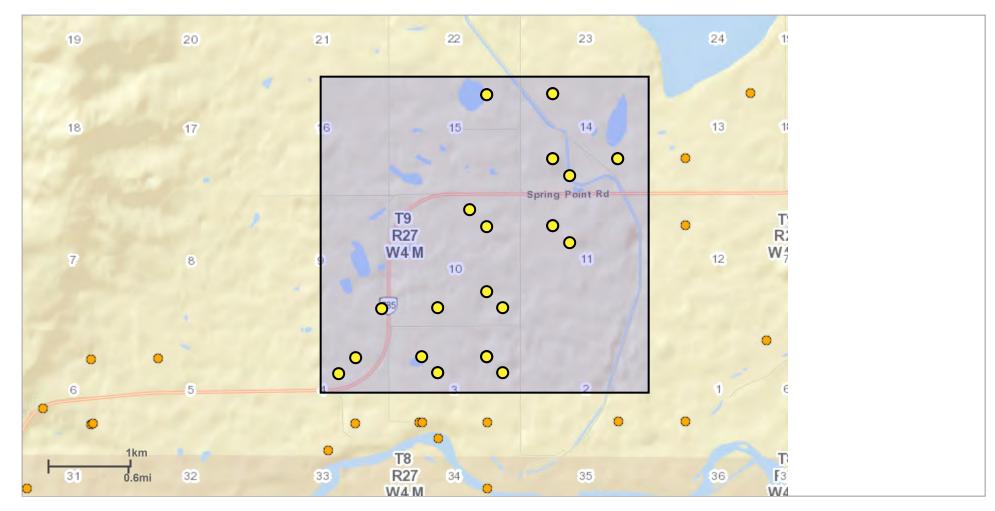
Alberta

Reconnaissance Report

View in Metric

Export to Excel

GIC Well ID	LSD	SEC	тwр	RGE	м	DRILLING COMPANY	DATE COMPLETED	DEPTH (ft)	TYPE OF WORK	USE	СНМ	LT	РТ	WELL OWNER	STATIC LEVEL (ft)	TEST RATE (igpm)	SC_DIA (in)
<u>115751</u>	NE	15	9	27	4	CAMFIELD DRILLING SERVICES LTD.	1988-04-09	90.00	New Well	Stock		5		DERSCH RANCH	80.00	50.00	6.63
<u>155266</u>	NE	3	9	27	4	UNKNOWN DRILLER		0.00	Chemistry	Domestic	1			ELLIOTT, TODD/CONNIE			0.00
<u>155267</u>	SW	14	9	27	4	UNKNOWN DRILLER		100.00	Chemistry	Domestic	<u>4</u>			CLAYPOOL, LINDA			0.00
<u>244439</u>	SE	14	9	27	4	UNKNOWN DRILLER		0.00	Chemistry	Domestic	<u>1</u>			HERWEYER, PETER			0.00
<u>250831</u>	1	9	9	27	4	STAVELY WATER WELLS	1994-11-25	113.00	New Well	Domestic		10	25	2B CATTLE CO LTD	93.80	2.00	6.62
<u>1250852</u>	NE	15	9	27	4	DOLLMAN'S WATER WELL DRILLING INC.	2019-01-24	100.00	New Well	Domestic		3	26	DEWIT, HENDRIK	54.46	75.00	
<u>2093787</u>	SE	10	9	27	4	UNKNOWNDRILLINGCOMP11	1978-11-05	13.00	Well Inventory	Domestic & Stock		1		NEELS, GERALD			



Alberta Water Well Information Database Map

Projection Web Mercator (Auxillary Sphere) Datum WGS 84 Date 11/19/2020, 1:41:50 PM

Legend

- Groundwater Drilling Report
- Baseline Water Well Report

http://groundwater.alberta.ca/WaterWells/d/

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11/19/2020

Print Module

Appendix E

Water Well Reports within 1.6km of the Site with a well depth equal to or less than 20 feet (including 0 feet) and associated chemistry results



The driller supplies the data contained in this report. The Province disclaims responsibility for its

View in Metric Export to Excel 115717

GoA Well Tag No.

GIC Well ID

GOWN ID	on this report will be retained in a publi	ic database.	Drilling Company Well Date Report Received	
Well Identification and Location				leasurement in Imperial
Owner Name Address VAN WAARDHUIZEN, PETER	Town	Province		Postal Code
Location1/4 or LSDSECTWPRGENE3927	W of MER Lot 4	Block Plan Additio	nal Description	
Measured from Boundary of ft from ft from	GPS Coordinates in Decima Latitude <u>49.709528</u> How Location Obtained Not Verified	al Degrees (NAD 83) Longitude <u>-113.575396</u>	Elevation 32 How Elevation Obtain Estimated	30.00 ft
Drilling Information				
Drilling Information Method of Drilling Hand Dug Proposed Well Use Demostic	Type of Work Chemistry			
Domestic Formation Log Mea	asurement in Imperial Y	ield Test Summary	M	easurement in Imperial
Depth from ground level (ft) Bearing		Recommended Pump Rate Test Date Water Removal	igpm	tatic Water Level (ft)
	70 5.	Vell Completion otal Depth Drilled Finished Wel 00 ft Borehole		easurement in Imperial End Date
		Diameter (in) 0.00	From (ft) 0.00	To (ft) 5.00
	S	urface Casing (if applicable)	Well Casing/Li	ner
		Size OD : 0.00 in		
		Wall Thickness : 0.000 in Bottom at : 0.00 ft		s : 0.000 in at : 0.00 ft
		<u> </u>	Bottom a	
	P	Perforations		
		From (ft) To (ft) Slot Wid		Hole or Slot Interval(in)
		Perforated by		
	A	nnular Seal Placed from 0.00 ft Amount	to 0.00 ft	
	0	ther Seals Type		At (ft)
	s	creen Type Size OD :0.00 in	1	
		From (ft)	To (ft)	Slot Size (in)
		Attachment		
	P	Top Fittings	Bottom Fitting	IS
		Type Amount	Grain Size	
Contractor Certification				
Name of Journeyman responsible for drilling/construction of UNKNOWN NA DRILLER	^r well	Certification No 1		

Company Name UNKNOWN DRILLER Copy of Well report provided to owner Date approval holder signed



Alberta Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its

View in Metric Export to Excel 115717

GIC Well ID GoA Well Tag No.

GOWN ID		ac	curacy. The infe	ormation on t	this report will be	retained in a p	ublic databa	se.		Drilling Compa Date Report F		1978/02/22
Well Identi	ification and L	ocation									Meas	urement in Imperial
<mark>Owner Nam</mark> VAN WAAR	ne RDHUIZEN, PEI	TER	Address			Town			Province	Сол	untry	Postal Code
Location	1/4 or LSD NE	SEC 3	TWP 9	RGE 27	W of MER 4	Lot	Block	Plan		nal Description		
Measured fi		of ft from ft from			GPS Coordin Latitude How Locatio Not Verified	49.709528 on Obtained	0			Elevation How Elevatio Estimated	3230.0 on Obtained	<u>0 ft</u>
Additional	Information										Meas	urement in Imperial
	From Top of Cas n Flow Pato	0			in	ls	s Flow Cor	ntrol Installed				
Decement	Rate		igpm			Duran	1			Derette		
	nded Pump Rat nded Pump Inta		From TOC)		igpm ft		_		Make	Depth Model (Out	ft H.P tput Rating)	
Did you E	Encounter Salin	e Water (>		DS) Gas		h		Geo		n Completion g Taken o ESRD		
Addition	nal Comments o	n Well					Sample C	ollected for F	^o otability		Submitted to	ESRD <u>Yes</u>
Yield Test								Tal	ken From (Ground Level	Meas	urement in Imperia
Test Date		Start Tim	е	Static	Water Level ft	_						
Method of	f Water Remov											
F	Removal Rate											
	thdrawn From											
lf water ren	moval period wa	as < 2 hour	s, explain wh	V								
Water Dive	erted for Drillin	ng										
Water Sour	rce	-		Amo	unt Taken ie	ig			Diversio	on Date & Time		

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed



CHEMICAL ANALYSIS REPORT

WELL NAME LOCATION WELL DEPTH AQUIFER SAMPLING DATE	VAN WAARDHUIZEN, PETER LSD NE SEC 3 TWP 9 5.00 ft 1978-02-20	RG 27 M 4		15717 664 ft E	
FIELD BICARBONATE CHLORIDE DISSOLVED OXYGEN IRON PH S2		1G/L	FIELD CARBONATE CONDUCTIVITY EH MANGANESE SULPHATE TEMPERATURE(C)		MG/L 0
TOTAL ALKALINITY			TOTAL HARDNESS		
LABORATORY COD DIC ION BALANCE SAR TOTAL ALKALINITY TDS	1.0 452.0	0500 0000 446	Analysis Date 197 CONDUCTIVITY FLUORIDE PH SIO2 TC TN	8-02-27	832 0.7100 7.90 8.3000
DOC AMMONIUM-N			BICARBONATE		551.0526
CALCIUM	43.9	9998	CARBONATE		
CHLORIDE	6.0	0102	MAGNESIUM		72.0589
NITRATE-N			NITRITE-N		-0.0994
PHOSPHATE SODIUM	39.0	9993	POTASSIUM SULPHATE		3.1720 -10.0144
NO2 + NO3		0994	TOTAL HARDNESS		404.0000
ALUMINUM BARIUM CADMIUM COBALT IRON MANGANESE MOLYBDENUM SELENIUM VANADIUM		2800	ARSENIC BERYLLIUM CHROMIUM COPPER LEAD MERCURY NICKEL STRONTIUM ZINC		
HYDROCARBONS PHENOLICS			PESTICIDES		

Remarks:

Temperature reported in Degree Centigrade. Conductivity reported in microsiemens/cm, pH in pH units. Alkalinity and Hardness expressed as Calcium Carbonate. FE, VA, PB, AL, AG expressed as extractable. FE in field measurements and all remaining metals expressed as total. '-' indicates concentrations less than.

EH	- Oxidation-Reduction Potential	SAR	- Sodium Adsorption Ratio	DIC	- Dissolved Inorganic Carbon
COD	- Chemical Oxygen Demand	DOC	- Dissolved Organic Carbon	ΤN	- Total Particulate Nitrogen
TDS	- Total Dissolved Solids	тс	- Total Particulate Carbon		

Note: this data may not be fully checked. The Province disclaims all responsibility for its accuracy



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View in Metric Export to Excel 115719

GoA Well Tag No. Drilling Company Well ID

GIC Well ID

4000/00/45

OWN ID	accuracy. The information	n on this report will be retained	d in a public database.		Report Received	, 1980/09/15
Well Identification and	Location				•	asurement in Imperi
Owner Name SIEBERT, JOHN	Address P.O. BOX 1914		Town FT. MACLEOD	Province ALBERTA	Country CANADA	Postal Code T0L 0Z0
Location 1/4 or LSD NE	SEC TWP RGE 3 9 27	W of MER Lo	ot Block Plan	Additional De	escription	
Measured from Boundary				3.575396 Elev How	vation <u>3300</u> . v Elevation Obtained mated	.00 ft
Drilling Information						
Method of Drilling Hand Dug		Type of Work Chemistry				
Proposed Well Use Domestic						
Formation Log	Μ	easurement in Imperia		-	Mea	asurement in Imper
Depth from Water ground level (ft) Bearing	Lithology Description			mp Rate Water Removal Rate	igpm (igpm) Stati	ic Water Level (ft)
			Well Completion Total Depth Drilled 20.00 ft	Finished Well Dept		asurement in Imper End Date
			Borehole Diameter (in) 0.00 Surface Casing (if	0	m (ft) .00 Well Casing/Line	To (ft) 20.00
			Wall Thickness :	in in ft	Wall Thickness :	0.00 ft
			Perforations From (ft) To	(ft) Diameter or Slot Width(in)	Slot Length (in)	Hole or Slot Interval(in)
			Amount Other Seals	ft to	_	t (ft)
			Screen Type Size OD : From (ft)	in To) (ft)	Slot Size (in)
					Bottom Fittings	
			Pack Type Amount		Grain Size	
	<u></u>					
Contractor Certification Name of Journeyman resp UNKNOWN NA DRILLER	ponsible for drilling/construction	of well	Certificat 1	tion No		
Company Name				Well report provided	to owner Date ap	proval holder signed



GOWN ID

Water Well Drilling Report

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View in MetricExport to ExcelIC Well ID115719

GIC Well ID 115719 GoA Well Tag No. Drilling Company Well ID Date Report Received 1980/09/15 Measurement in Impe

Well Identifica	ation and Lo	ocation									Measure	ment in Imperia
<mark>Owner Name</mark> SIEBERT, JO⊦	HN		Address P.O. BOX	(1914		Towr FT. N	ACLEOD		Province ALBERTA	Count CANA	,	Postal Code T0L 0Z0
	1/4 or LSD NE	SEC 3	TWP 9	RGE 27	W of MER 4		Block	Plan		Description		
Measured from	1	f ft from ft from			Latitude	dinates in De 49.709528 tion Obtained	Long	ees (NAD 83) itude <u>-113.5</u>	75396 E	Elevation dow Elevation stimated	3300.00 ft Obtained	
Additional Inf	ormation										Measure	ment in Imperia
Distance Fron Is Artesian Fi R	n Top of Casi flow Rate				in	-						
Recommende Recommende	ed Pump Rate	Э			igp	om Pum Typ	p Installed		D Make	epth	ft H.P.	_
	-		-							Model (Outpu	t Rating)	
Did you Enc	counter Saline	e Water (>	⊳4000 ppm	TDS) Gas		oth		Geo	fected Upon Co physical Log Ta Submitted to E	aken		
THE FOLLOW							ROUNDWAT	TER TESTIN	Potability	APPLICATION	RECEIVED (ON JANUARY
SYSTEM.												
Yield Test Test Date		Start Tim	ie	Stati	c Water Level ft			Tał	ken From Gro	und Level	Measure	ment in Imperia
Method of Wa	Туре											
Rem Depth Withdr	noval Rate rawn From											
lf water remov	val period wa	s < 2 hour	rs, explain v	why								
Water Diverte	ed for Drillin	ng										
Water Source				Am	ount Taken	ig			Diversion L	Date & Time		

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	<i>Certification No</i> 1	
Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed



WELL NAME LOCATION WELL DEPTH AQUIFER SAMPLING DATE	SIEBERT, JOHN LSD NE SEC 3 20.00 ft 1980-09-12	TWP 9 RG 27 M 4	GIC WELL ID 115719 SAMPLE NO. 9918 WATER LEVEL LABORATORY AE	ft
FIELD BICARBONATE CHLORIDE DISSOLVED OXYGEN IRON PH S2	١	MG/L	FIELD CARBONATE CONDUCTIVITY EH MANGANESE SULPHATE TEMPERATURE(C)	MG/L 0
TOTAL ALKALINITY LABORATORY COD DIC ION BALANCE SAR TOTAL ALKALINITY TDS		1.0700 505.0000 489	TOTAL HARDNESS Analysis Date 1980-09-23 CONDUCTIVITY FLUORIDE PH SIO2 TC TN	869 0.7800 8.40 11.1000
DOC AMMONIUM-N CALCIUM CHLORIDE NITRATE-N PHOSPHATE SODIUM NO2 + NO3 ALUMINUM BARIUM CADMIUM COBALT IRON MANGANESE MOLYBDENUM SELENIUM VANADIUM		469 58.9998 3.0033 26.9997 -0.0504	IN BICARBONATE CARBONATE MAGNESIUM NITRITE-N POTASSIUM SULPHATE TOTAL HARDNESS ARSENIC BERYLLIUM CHROMIUM COPPER LEAD MERCURY NICKEL STRONTIUM ZINC	597.0601 9.0000 85.0701 -0.0504 1.7400 11.0149 496.0000
HYDROCARBONS PHENOLICS			PESTICIDES	

Remarks:

Temperature reported in Degree Centigrade. Conductivity reported in microsiemens/cm, pH in pH units. Alkalinity and Hardness expressed as Calcium Carbonate. FE, VA, PB, AL, AG expressed as extractable. FE in field measurements and all remaining metals expressed as total. '-' indicates concentrations less than.

EH	- Oxidation-Reduction Potential	SAR	- Sodium Adsorption Ratio	DIC	- Dissolved Inorganic Carbon
COD	- Chemical Oxygen Demand	DOC	- Dissolved Organic Carbon	TN	- Total Particulate Nitrogen
TDS	- Total Dissolved Solids	тс	- Total Particulate Carbon		

Note: this data may not be fully checked. The Province disclaims all responsibility for its accuracy



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155266

GoA Well Tag No. Drilling Company Well ID

GIC Well ID

View in Metric Export to Excel

GOWN ID		ac	curacy. The Info	rmation on 1	this report will be re	tained in a p	udiic database.			Date Report Re		1990/10/19
Well Identifi	cation and Lo	ocation									Meas	surement in Imperial
Owner Name ELLIOTT, TO			Address #124 21 BER	RKELY PL	, LETHBRIDGE	Town			Province	Coun	try	Postal Code T1K 5N1
Location	1/4 or LSD NE	SEC 3	TWP 9	RGE 27	W of MER 4	Lot	Block	Plan	Additio	nal Description		
Measured fro		t from t from			GPS Coordina Latitude <u>49</u> How Location Not Verified	.709528		(NAD 83) de <u>-113.5</u>		Elevation How Elevation Not Obtained	Obtained	ft
Drilling Infor Method of D Not Applicabl Proposed W	rilling e				Type of Work Chemistry							
Domestic Formation L	.og			Meas	urement in Imp	erial	Yield Test	Summar	ſy		Meas	surement in Imperia
Depth from ground level	Water	Litholog	y Description				Recommen Test Dat	ded Pump	Rate	igpm Rate (igpm)		Water Level (ft)
							0.00 ft		Finished Well	I Depth Start D		surement in Imperial End Date
								eter (in) .00 sing (if aj	pplicable)	From (ft) 0.00 Well Cas	ing/Liner	To (ft) 0.00
							Wall Thick	om at :	0.00 in 0.000 in 0.00 ft	Wall Th	ize OD : ckness : Top at : ttom at :	0.00 in 0.000 in 0.00 ft 0.00 ft
							From (ft) Perforated I	To (ft)	Diamete) Slot Wid			Hole or Slot Interval(in)
							Annular Se Placed fr Amo Other Seals	om unt	0.00 ft <i>t</i>	to <u>0.00</u>	ft	
								Туре	e		At	(ft)
								ə OD :	0.00 in			
								m (ft) ment		To (ft)		Slot Size (in)
							Top Fi Pack	ttings		Bottom	Fittings	
							Type Amount		00	Grain S	ize	
Contractor (Certification											
	rneyman respo	nsible for	drilling/constru	iction of w	vell		C 1	Certification	n No			

Company Name

UNKNOWN DRILLER

Copy of Well report provided to owner Date approval holder signed



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GoA Well Tag No.

Drilling Company Well ID

GIC Well ID

View in Metric Export to Excel 155266

OWN ID										Date Report Rec	eived	1990/10/19
Well Identi	fication and L	ocation									Mea	surement in Imperi
Owner Nam ELLIOTT, T	ODD/CONNIE		Address #124 21 BE	RKELY PL, I	ETHBRIDGE	Town			Province	Countr	У	Postal Code T1K 5N1
Location	1/4 or LSD NE	SEC 3	TWP 9	RGE 27	W of MER 4	Lot		Plan		nal Description		
Measured fi		of ft from ft from			GPS Coordina Latitude 49 How Location Not Verified	9.709528		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Elevation How Elevation (Not Obtained		
Additional	Information										Mea	surement in Imper
Distance F Is Artesiar	rom Top of Cas n Flow Rate				in	Is	Flow Con	trol Installed Describe				
	nded Pump Rate nded Pump Inta	е			igpm	Pump	Installed			Depth	H.P.	
Did you l	Encounter Salin	e Water (>		0S) Gas				Geop		Completion g Taken o ESRD		
Addition	al Comments or	n Well					Sample Co	ollected for Po	otability	SL	ıbmitted	to ESRD <u>Yes</u>
Yield Test								Take	en From G	Ground Level	Mea	surement in Impe
Test Date		Start Tim	е	Static V	Vater Level ft							
Method of	Water Remova Type _											
	Removal Rate		igpm									
	hdrawn From			Ŷ								
Water Dive	erted for Drillir	ng										
Water Sour	ce			Amoui	nt Taken ig				Diversio	n Date & Time		

ſ	Contractor Certification		
	Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
	Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed

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CHEMICAL ANALYSIS REPORT

WELL NAME LOCATION WELL DEPTH AQUIFER SAMPLING DATE	ELLIOTT, TODD/CONNIE LSD NE SEC 3 TWP 9 F 0.00 ft WELL 1990-10-09	RG 27 M 4	GIC WELL ID SAMPLE NO. WATER LEVEL LABORATORY	155266 9009354 AE	ft
FIELD BICARBONATE CHLORIDE DISSOLVED OXYGEN IRON PH S2		G/L	FIELD CARBONATE CONDUCTIVITY EH MANGANESE SULPHATE TEMPERATURE(C)		MG/L 0
TOTAL ALKALINITY			TOTAL HARDNESS		
LABORATORY COD DIC ION BALANCE SAR TOTAL ALKALINITY TDS	1.00		Analysis Date CONDUCTIVITY FLUORIDE PH SIO2 TC TN	1990-10-17	342 0.1800 8.13 5.9000
DOC AMMONIUM-N			BICARBONATE		188.0000
CALCIUM	46.00		CARBONATE		
	1.10	000	MAGNESIUM		15.0000
NITRATE-N PHOSPHATE			NITRITE-N POTASSIUM		-0.0010
SODIUM	7.00	000	SULPHATE		0.8000 25.0000
NO2 + NO3	0.12		TOTAL HARDNESS		177.0000
ALUMINUM BARIUM CADMIUM COBALT IRON MANGANESE MOLYBDENUM SELENIUM VANADIUM	-0.0		ARSENIC BERYLLIUM CHROMIUM COPPER LEAD MERCURY NICKEL STRONTIUM ZINC		
HYDROCARBONS PHENOLICS			PESTICIDES		

Remarks:

CATIONS - 3.85 ANIONS - 3.65

Temperature reported in Degree Centigrade. Conductivity reported in microsiemens/cm, pH in pH units. Alkalinity and Hardness expressed as Calcium Carbonate. FE, VA, PB, AL, AG expressed as extractable. FE in field measurements and all remaining metals expressed as total. '-' indicates concentrations less than.

EH	- Oxidation-Reduction Potential	SAR	- Sodium Adsorption Ratio	DIC	- Dissolved Inorganic Carbon
COD	- Chemical Oxygen Demand	DOC	- Dissolved Organic Carbon	ΤN	- Total Particulate Nitrogen
TDS	- Total Dissolved Solids	тс	- Total Particulate Carbon		

Note: this data may not be fully checked. The Province disclaims all responsibility for its accuracy



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View in Metric Export to Excel 2093787

GoA Well Tag No. Drilling Company Well ID

GIC Well ID

Date Report Received 1985/09/10

GOWN ID	on this report will be retained in a	i public database.		Date Report Re	
Well Identification and Location					Measurement in Imperial
Owner NameAddressNEELS, GERALDP.O. BOX 881	Tow. FOR	n T MACLEOD	Province ALBERTA	Coun CAN/	
Location1/4 or LSDSECTWPRGESE10927	4	Block Plai		nal Description	
Measured from Boundary of ft from ft from	GPS Coordinates in De Latitude 49.716746 How Location Obtained Not Verified	Longitude -1	· · · · · · · · · · · · · · · · · · ·	Elevation How Elevation Not Obtained	
Drilling Information Method of Drilling Unknown Proposed Well Use Domestic & Stock	Type of Work Well Inventory				
	easurement in Imperial	Yield Test Sum	nmarv		Measurement in Imperial
Depth from Water ground level (ft) Bearing 13.00 Unknown			Pump Rate Water Removal		Static Water Level (ft)
		Well Completic Total Depth Drille 13.00 ft Borehole	on ed Finished Well	Depth Start D 1978/1	
		Diameter	(in)	From (ft)	To (ft)
		Surface Casing			sing/Liner
		Size OD Wall Thickness	: <u>in</u> :: in	 Wall Th	Size OD : in in in
		Bottom at	f: ft	_	Top at : ft
		Perforations		Bo	ottom at : ft
			Diamete o (ft) Slot Widt		
		Amount	ft t		
			Туре		At (ft)
		From (ft		To (ft)	Slot Size (in)
		Attachmen Top Fittings	s	Bottom	n Fittings
		Pack Type Amount		Grain S	Size
Contractor Certification					
Name of Journeyman responsible for drilling/construction UNKNOWN DRILLER11	of well	Certifi 11	cation No		
Company Name UNKNOWNDRILLINGCOMP11			of Well report prov	vided to owner	Date approval holder signed



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View in Metric Export to Excel 2093787

GoA Well Tag No. Drilling Company Well ID

GIC Well ID

1985/09/10

GOWN ID	accuracy. The In	formation on this report	will be retained in a	public database	е.		Report Received	1985/09/10
Well Identification and Loc	ation						Me	asurement in Imperia
Owner Name NEELS, GERALD	Address P.O. BOX 8	381	Tow. FOR	n T MACLEOD	1	Province ALBERTA	Country CANADA	Postal Code T0L 0Z0
	SEC TWP 10 9	RGE W of N 27 4		Block	Plan	Additional Des	scription	
	rom	Latitud	Coordinates in De le <u>49.716746</u> ocation Obtained	Longit		5400 Eleva How	ation Elevation Obtaine Dbtained	
Additional Information							Mea	asurement in Imperia
Distance From Top of Casing Is Artesian Flow Rate			<u>1</u>					
Recommended Pump Rate			igpm Pun	np Installed				
Recommended Pump Intake	Depth (From TOC)			pe		Make	, H.P	<u> </u>
, , , , , , , , , , , , , , , , , , ,							del (Output Rating)
Did you Encounter Saline V		DS) Gas	Depth Depth	ft ft	Geop		1	
Additional Comments on V INFORMATION FOR THIS V APPLICATION (1985/09/10), GRAVEL OUT OF THE BOT	ELL WAS OBTAINE PRIOR TO 1984 TI			NDWATER TE	ESTING & FA		- PLETION PROGRA	
Yield Test	,				Take		tlovel Me	asurement in Imperia
	tart Time	Static Water Le	evel ft		Take			
Method of Water Removal								
Removal Rate								
Depth Withdrawn From	ft							
If water removal period was <	< 2 hours, explain wh	<i>iy</i>						
Water Diverted for Drilling								
Water Source		Amount Take	n ig			Diversion Date	& Time	

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN DRILLER11	Certification No 11	
Company Name UNKNOWNDRILLINGCOMP11	Copy of Well report provided to owner	Date approval holder signed



The driller supplies the data contained in this report. The Province disclaims responsibility for its

View in Metric Export to Excel 115734

GoA Well Tag No. Drilling Company Well ID

GIC Well ID

GOWN ID accuracy. The information on	this report will be retained in a p	oublic database.	Date Report Received	1980/01/17
Well Identification and Location				easurement in Imperial
Owner Name Address VAN WAARDHUIZEN, PETER P.O. BOX 73 FT MAC	Town	Province	Country	Postal Code
Location 1/4 or LSD SEC TWP RGE NE 10 9 27	W of MER Lot 4	Block Plan Additio	onal Description	
Measured from Boundary of ft from	GPS Coordinates in Dec Latitude 49.724009 How Location Obtained	imal Degrees (NAD 83) Longitude <u>-113.575461</u>	Elevation <u>322</u> How Elevation Obtained	5.00 ft
ft from	Map		Estimated	ea
Drilling Information				
Method of Drilling Hand Dug	Type of Work Chemistry			
Proposed Well Use Domestic				
	urement in Imperial	Yield Test Summary		easurement in Imperial
Depth from Water ground level (ft) Bearing		Recommended Pump Rate Test Date Water Remova		tic Water Level (ft)
		Well Completion	Me	asurement in Imperial
		Total Depth Drilled Finished We		End Date
		Borehole Diameter (in)	From (ft)	To (ft)
		0.00	0.00	15.00
		Surface Casing (if applicable)	Well Casing/Lin	er
		Size OD : 0.00 in	n Size OD	: 0.00 in
		Wall Thickness : 0.000 in		
		Bottom at : 0.00 ft	t Top at Bottom at	
		Perforations		
		From (ft) To (ft) Slot Wid		Hole or Slot Interval(in)
		Perforated by		
		Annular Seal Placed from 0.00 ft	to 0.00 ft	
		Amount		
		Other Seals		A+ (f+)
		Туре		At (ft)
		Screen Type Size OD :0.00 ir	1	
		From (ft)	To (ft)	Slot Size (in)
		Attachment		
		Top Fittings	Bottom Fittings	
		Pack Type Amount	Grain Size	
		, anount		
Contractor Certification				
Name of Journeyman responsible for drilling/construction of v	vell	Certification No		

UNKNOWN DRILLER

Company Name

Copy of Well report provided to owner Date approval holder signed



The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

GoA Well Tag No.

View in Metric Export to Excel

Drilling Company Well ID

GIC Well ID

115734

1980/01/17

GOWN ID		а	ccuracy. The inf	ormation or	n this report will be	retained in a p	oublic databas	se.		Date Report Re		1980/01/17
Well Ident	ification and L	ocation									Measu	rement in Imperia
<mark>Owner Nan</mark> VAN WAAF	ne RDHUIZEN, PEI	ΓER	Address P.O. BOX 7	3 FT MAC	CLEOD	Town			Province	Cour	ntry	Postal Code
Location	1/4 or LSD NE	SEC 10	TWP 9	RGE 27	W of MER 4	Lot	Block	Plan	Additio	nal Description		
Measured f		of ft from ft from			GPS Coordi Latitude How Locatic Map	49.724009	Longi			Elevation How Elevation Estimated) ft
Additional	Information										Measu	rement in Imperia
Distance F Is Artesia	From Top of Cas In Flow Rate				in	I	's Flow Con	trol Installeo Describe				
	nded Pump Rat nded Pump Inta	e			igpm ft		o Installed e			Depth Model (Outp	ft <i>H.P.</i>	
Did you	Encounter Salin	e Water (>		DS) Gas	Depti Depti	h		Geo		Completion		
Addition	al Comments o	n Well					Sample Co	ollected for F	Potability		Submitted to	ESRD <u>Yes</u>
Yield Test								Tal	ken From (Ground Level	Measu	rement in Imperia
Test Date		Start Tin	пе	Stati	ic Water Level ft							·
	f Water Remov Type Removal Rate		igpm									
	thdrawn From											
lf water rei	moval period wa	as < 2 hou	rs, explain wh	У								
Water Div	erted for Drillin	ng										
Water Sour	rce			Am	ount Taken	a			Diversio	on Date & Time		

ſ	Contractor Certification		
	Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
	Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed



CHEMICAL ANALYSIS REPORT

WELL NAME LOCATION WELL DEPTH AQUIFER SAMPLING DATE	VAN WAARDHUIZEN, PETER LSD NE SEC 10 TWP 9 RG 27 M 15.00 ft 1980-01-11	GIC WELL ID 115734 1 4 SAMPLE NO. 446 WATER LEVEL ft LABORATORY AE	
FIELD BICARBONATE CHLORIDE DISSOLVED OXYGEN IRON PH S2	MG/L	FIELD CARBONATE CONDUCTIVITY EH MANGANESE SULPHATE TEMPERATURE(C)	MG/L 0
TOTAL ALKALINITY		TOTAL HARDNESS Analysis Date 1980-01-22	
COD DIC		CONDUCTIVITY FLUORIDE	772 0.3200
ION BALANCE SAR	1.0300	PH SIO2	8.30 9.6000
TOTAL ALKALINITY TDS DOC	425.0000 461	TC TN	
AMMONIUM-N CALCIUM	61.9998	BICARBONATE CARBONATE	518.0497
CHLORIDE NITRATE-N	3.0033	MAGNESIUM NITRITE-N	57.0474 -0.0504
PHOSPHATE SODIUM	40.9998	POTASSIUM SULPHATE	3.5800 24.0356
NO2 + NO3 ALUMINUM BARIUM CADMIUM COBALT IRON MANGANESE MOLYBDENUM SELENIUM VANADIUM	3.4370 0.0200	TOTAL HARDNESS ARSENIC BERYLLIUM CHROMIUM COPPER LEAD MERCURY NICKEL STRONTIUM ZINC	388.0000
HYDROCARBONS PHENOLICS		PESTICIDES	

Remarks:

Temperature reported in Degree Centigrade. Conductivity reported in microsiemens/cm, pH in pH units. Alkalinity and Hardness expressed as Calcium Carbonate. FE, VA, PB, AL, AG expressed as extractable. FE in field measurements and all remaining metals expressed as total. '-' indicates concentrations less than.

EH	- Oxidation-Reduction Potential	SAR	- Sodium Adsorption Ratio	DIC	- Dissolved Inorganic Carbon
COD	- Chemical Oxygen Demand	DOC	- Dissolved Organic Carbon	ΤN	- Total Particulate Nitrogen
TDS	- Total Dissolved Solids	тс	- Total Particulate Carbon		

Note: this data may not be fully checked. The Province disclaims all responsibility for its accuracy



The driller supplies the data contained in this report. The Province disclaims responsibility for its

GIC Well ID GoA Well Tag No.

Drilling Company Well ID

244439

View in Metric Export to Excel

SOWN ID		a	ccuracy. The in	formation o	on this report will be	retained in a p	ublic databas	e.		Date Report Received	
Well Identi	fication and Lo	ocation								Ν	Measurement in Imperia
Owner Nam HERWEYEF			Address P.O. BOX 6	687 FOR ¹	T MACLEOD	Town			Province	Country	Postal Code T0L 0Z0
Location	1/4 or LSD SE	<i>SEC</i> 14	TWP 9	RGE 27	W of MER 4	Lot	Block	Plan		nal Description	
Measured fr		f ft from ft from				inates in Dec 49.731485 on Obtained		es (NAD 83) itude113.5	·	Elevation How Elevation Obtain Not Obtained	ft
Drilling Info Method of L Unknown					<i>Type of Wo</i> Chemistry	ork					
Proposed V Domestic	Vell Use										
Formation Depth from ground level	Water	Litholog	gy Description		asurement in In		Recomme Test Da Vell Con Total Depu 0.00 ft Borehole Diar Surface C Surface	mpletion th Drilled F meter (in) 0.00 Casing (if a) ize OD : ckness : ttom at : ons) To (ft) Seal from nount als Type ize OD : rom (ft) chment	p Rate	igpm Rate (igpm) S Pepth Start Date From (ft) 0.00 I Well Casing/L Size 0 Wall Thicknes Top Bottom o 0.00 ft in or th(in) I o 0.00 ft in or th(in) I o 0.00 ft	DD : 0.00 in ss : 0.000 in at : 0.00 ft
							Pack Type Amount			Grain Size	
Contractor	Certification										
	urneyman respo	nsible for	r drilling/cons	truction of	f well			Certificatio	on No		
UNKNOWN Company N	NA DRILLER							1 Copv of W	ell report prov	vided to owner Date	e approval holder signed

UNKNOWN DRILLER



Alberta Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its

GIC Well ID GoA Well Tag No.

View in Metric Export to Excel

244439

OWN ID		a	ccuracy. The in	formation on	this report will be re	etained in a public da	itabase.	, .	Drilling Compar Date Report Re		1987/05/25
Well Ident	ification and L	ocation								Meas	surement in Imperia
Owner Nam HERWEYE	ne R, PETER		Address P.O. BOX	687 FORT	MACLEOD	Town		Province	Cour	ntry	Postal Code T0L 0Z0
Location	1/4 or LSD SE	SEC 14	TWP 9	RGE 27	W of MER 4	Lot Blo	ck Plan	Additio	nal Description		
Measured f	from Boundary o	of ft from ft from				ates in Decimal D 0.731485 L Obtained			Elevation How Elevation Not Obtained		ft
Additional	Information									Meas	urement in Imperia
	From Top of Cas				in	Is Flow	Control Installe				
	Rate		igpm								
	nded Pump Rai nded Pump Inta		(From TOC)		igpm ft		lled			H.P.	
									Model (Outp	ut Rating)	
Did you l	Encounter Salir	ie Water (>		DS) Gas		ft ft			g Taken		
	al Comments o LY NO LSD	n Well				Samp	le Collected for	Potability		Submitted t	o ESRD <u>Yes</u>
Yield Test							Ta	aken From C	Ground Level	Meas	surement in Imperia
Test Date		Start Tim	те	Statio	c Water Level ft						
Method of	f Water Remov Type										
F	Removal Rate					_					
	thdrawn From										
lf water rer	moval period wa	as < 2 houi	rs, explain wl	hy							
Water Div	erted for Drilli	ng									
Water Sour	rce			Amo	ount Taken ig			Diversio	on Date & Time		

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
Company Name UNKNOWN DRILLER	Copy of Well report provided to owner	Date approval holder signed



CHEMICAL ANALYSIS REPORT

WELL NAME LOCATION WELL DEPTH AQUIFER SAMPLING DATE	HERWEYER, PETER LSD SE SEC 14 TWP 9 RG 27 M 4 0.00 ft WELL 1987-04-16	GIC WELL ID 244439 SAMPLE NO. 121 WATER LEVEL ft LABORATORY AE	
FIELD BICARBONATE CHLORIDE DISSOLVED OXYGEN IRON PH S2	MG/L	FIELD CARBONATE CONDUCTIVITY EH MANGANESE SULPHATE TEMPERATURE(C)	MG/L 0
TOTAL ALKALINITY		TOTAL HARDNESS	
LABORATORY COD DIC ION BALANCE SAR	1.0000	Analysis Date 1987-05-11 CONDUCTIVITY FLUORIDE PH SIO2	440 0.3300 7.01
TOTAL ALKALINITY	213.0000 268	TC TN	
DOC AMMONIUM-N CALCIUM CHLORIDE NITRATE-N PHOSPHATE	0.1400 46.0000 0.9000	BICARBONATE CARBONATE MAGNESIUM NITRITE-N POTASSIUM	260.0000 16.0000 2.0000
SODIUM	32.0000	SULPHATE	43.0000
NO2 + NO3 ALUMINUM BARIUM CADMIUM COBALT IRON MANGANESE MOLYBDENUM SELENIUM VANADIUM	-0.0700 1.2200	TOTAL HARDNESS ARSENIC BERYLLIUM CHROMIUM COPPER LEAD MERCURY NICKEL STRONTIUM ZINC	182.0000
HYDROCARBONS PHENOLICS		PESTICIDES	

Remarks:

Temperature reported in Degree Centigrade. Conductivity reported in microsiemens/cm, pH in pH units. Alkalinity and Hardness expressed as Calcium Carbonate. FE, VA, PB, AL, AG expressed as extractable. FE in field measurements and all remaining metals expressed as total. '-' indicates concentrations less than.

EH	- Oxidation-Reduction Potential	SAR	- Sodium Adsorption Ratio	DIC	- Dissolved Inorganic Carbon
COD	- Chemical Oxygen Demand	DOC	- Dissolved Organic Carbon	TN	- Total Particulate Nitrogen
TDS	- Total Dissolved Solids	тс	- Total Particulate Carbon		

Note: this data may not be fully checked. The Province disclaims all responsibility for its accuracy



The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

GIC Well ID GoA Well Tag No.

Drilling Company Well ID

115750

View in Metric Export to Excel

GOWN ID		а	ccuracy. The in	formation on	this report will be retained in a	a public database.			Report Receive	
Well Identifica	ation and Lo	cation								Measurement in Imperial
Owner Name GROUNDWAT T	ER INVEST. ;	#5067-	Address		Том	in	Pro	ovince	Country	Postal Code
	/4 or LSD W	SEC 14	TWP 9	RGE 27	W of MER Lot 4			Additional De	escription	
Measured from	ft	t from t from			GPS Coordinates in Do Latitude <u>49.738716</u> How Location Obtained Not Verified	Longitude	NAD 83) ∋113.564025	How	vation w Elevation Obta	
Drilling Inform	ation									
Method of Dril Auger					Type of Work Test Hole					
Proposed Well Unknown										
Formation Lo	g			Meas	surement in Imperial	Yield Test S	Summary			Measurement in Imperial
Depth from ground level (ft	Water) Bearing	Litholog	gy Descriptior	۱		Recommende Test Date	ed Pump Rate Water Re	emoval Rate	igpm (igpm)	Static Water Level (ft)
2.00		Grave								
7.00		Silty C	,			Well Comple				Measurement in Imperial
11.00			m Grained Sa	nd		Total Depth D 13.00 ft	Drilled Finishe	ed Well Depi	th Start Date 1986/09/11	End Date 1986/09/11
13.00		Silty C	lay			Borehole			1000/00/	
						Size Wall Thickne Botton Perforations From (ft) Perforated by Annular Seal Placed fror Amour Other Seals Screen Type Size	00 ing (if applica 0D : 0 0ess : 0.0 m at : 0 To (ft) SI M 0.00 m 0.00 mt 0.00 mt 0.00 mt 0.00 mt 0.00 0D : 0 0n (ft) 0	0.00 in 0.00 ft 0.00 ft 0.00 ft 0.00 ft 0.00 ft 0.00 in 0.00 in	Bottom Slot Length	OD : 2.00 in ess : 1.063 in o at : 0.00 ft
						Attachm Top Fitti Pack Type Amount	ings			ngs
Contractor Ce	rtification									
Name of Journe UNKNOWN NA		nsible for	r drilling/const	truction of v	well	Ce 1	ertification No			
Company Nam							py of Well rep	ort provided	to owner Dat	te approval holder signed

ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION



Water Source

GOWN ID

Alberta Water Well Drilling Report

GIC Well ID GoA Well Tag No.

View in Metric Export to Excel 115750

OWN ID					this report will be					Drilling Compa Date Report R		
Well Iden	tification and L	ocation									Meas	urement in Imperial
Owner Nar GROUND\ T	<mark>me</mark> WATER INVEST	. #5067-	Address			Town			Province	Сог	Intry	Postal Code
Location	1/4 or LSD NW	SEC 14	TWP 9	RGE 27	W of MER 4	Lot	Block	Plan		nal Description		
Measured		f ft from ft from				19.738716	•	ees (NAD 83) iitude <u>-113.56</u>		Elevation How Elevatio	on Obtained	ft
Additiona	I Information										Meas	urement in Imperial
	From Top of Cas an Flow Rate	-			in		ls Flow Coi	ntrol Installed Describe				
Recomme	ended Pump Rate	е			igpm	Pum	o Installed				ft	
Recomme	ended Pump Inta	ke Deptł	(From TOC)		ft	Тур	9		Make		H.P. put Rating)	
Did you	Encounter Salin	e Water		DS) Gas		ז ז	ft ft	Geoj		n Completion g Taken o ESRD		
Additio	nal Comments or	n Well					Sample C	Collected for P	Potability		Submitted to) ESRD
Yield Tes	t							Tak	en From C	Ground Level	Meas	urement in Imperial

Diversion Date & Time

Test Date	Start Time	Static Water Level ft		
Method of Water R	emoval		-	
Т	уре			
Removal F	Rate igp	m		
Depth Withdrawn F				

Amount Taken

ig

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
Company Name ALBERTA ENVIRONMENT/EARTH SCIENCES DIVISION	Copy of Well report provided to owner	Date approval holder signed

Appendix F

Site Borehole Logs and Locations

advanced August 9, 2019

CHILAKO DRILLING SERVICES LTD

Box 942 Coaldale, Alberta, T1M 1M8 (403) 345-3710

SOIL PROFILE AND PARENT MATERIAL DESCRIPTION

Site Location: Arie Muilwijk

Date: 09-Aug-19

Hole #	Location	Depth	Texture	Moisture	Geological	Sample	Remarks
AM1-19	0314346	0-2.1	VFSL	SM	Lac		Silty
	5511364	2.1-3.5	VFSCL	VM	Lac		
		3.5-5.1	VFSL	VM-Sat	Lac		
		5.1-5.9	SiCL	М	Lac		V. firm, med-high plastic, yellow brown
		5.9-6.2	FSCL	VM	Lac		Slough @ 3.3m
AM2-19	0314354	0-2.9	VFSL	SM	Lac		Silty
	5511400	2.9-3.6	SiCL	VM	Lac		Sandy
		3.6-5.6	VFSL	Sat	Lac		Soft, olive brown, silty, free water
		5.6-6.2	SiCL	М	Lac		V. firm, med-high plastic, olive brown
							slough @ 3.9m
AM3-19	0314364	0-1.8	VFSL	М	Lac		Loose, olive brown, silty
	5511294	1.8-2.3	VFSCL	VM	Lac		Low plastic, olive brown, silty
		2.3-3.0	VFSL	VM	Lac		Silty
		3.0-4.1	VFSL	Sat	Lac		Silty, free water, VFSL sand lenses
		4.1-4.6	SiCL	М	Lac		Stiff, med plastic, olive brown
		4.6-5.0	VFSCL	VM	Lac		Soft, low plastic, olive brown
		5.0-6.2	SiCL	VM	Lac		Firm, low plastic, olive brown
AM4-19	0314411	0-1.0	SiCL	М	Lac		
_	5511281	1.0-2.7	VFSL	М	Lac		
		2.7-4.4	VFSL	Sat	Lac		Soft
		4.4-6.2	C-SC	М	Till		Stiff, low plastic, trace gravel

Legend: L

L Loam C Clay S Sand Gr. Gravel Si Silt F Fine (sand) VF Very Fine (sand)

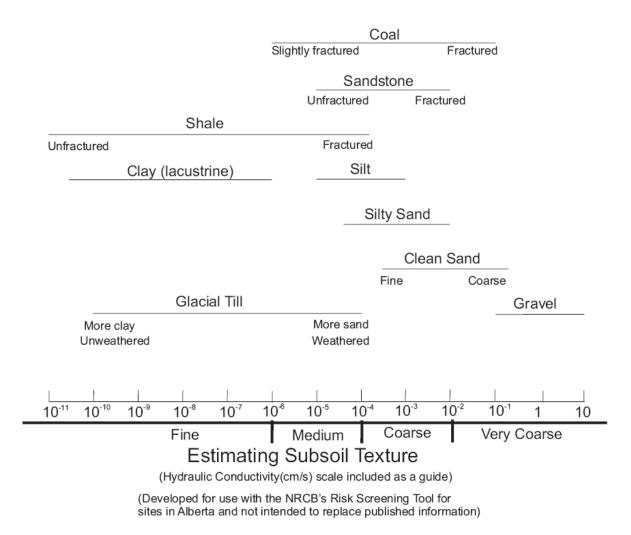
Eg. VFSCL = Very Fine Sandy Clay Loam



Appendix G

Environmental Risk Screening Tool

Estimating Subsoil Texture



AO: Protective Layer Report prepared as part of the ERST Scoring

LA19036 Site Information Form Supporting Information Protective Layer (PL) – NE 10-9-27 W4

The Environmental Risk Screening Tool, version 1.2, September 2011, page 11, (Appendix A) states:

Predominant Geology of the PL – Using the most site specific information; indicate the geology of the protective layer. If the material is very heterogeneous (i.e. multiple layers of different geologic materials), then the dominant geologic unit that has the lowest hydraulic conductivity should be considered.

The most site specific information is the four borehole logs (Appendix B). SiCL (silty clay loam) from 0.9 to 1.0m thick was found above the uppermost groundwater resource (UGR) in AM2-19 and AM4-19 and would have the lowest hydraulic conductivity of soils located above the UGR.

However, VFSL (very fine sandy loam) is found in all four boreholes above the UGR. Therefore, I find it to be the dominant geologic unit on site above the UGR, so is the best choice for the Protective Layer.

Reference: borehole AM4-19 Predominant geology: very fine sandy loam [1.0 m to 2.7m] PL measured From: 1.0m PL measured To: 2.7m Subsoil Texture: Coarse

The subsoils texture is chosen as coarse because this is the same lithology as the UGR, and coarse was the texture choice for the UGR.

Scott Cunningham

Scott Cunningham, P.Eng, P.Ag.

December 3, 2020

Appendix A – Environmental Risk Screening Tool (page 11) Appendix B – Site Borehole Logs and Locations Appendix A

Environmental Risk Screening Tool

Companion document, page 11

medium, coarse or very coarse). For example, a gravel UGR would be assigned a "very coarse" subsoil texture using the table. For reference, a hydraulic conductivity scale is also included in the table to allow for estimating of hydraulic conductivity. If a shale UGR has been identified, the shale should be considered as fractured.

9. Protective Layer (PL)

- Reference(s) for protective layer (PL) Indicate what sources of information were
 used to determine the PL. For example, indicate the well I.D.s of the well logs used
 (could include information from decommissioned, chemistry and well inventory logs)
 or information on other boreholes in the area of the facility that were used.
- Thickness of PL Protective layers are geologic units that generally have a low hydraulic conductivity (e.g. unfractured glacial till) overlying a UGR. These layers can be identified by examining water well drillers logs or site specific geotechnical information. At a facility where a liner has been constructed, use the native subsoil under the facility when determining the protective layer thickness – not the liner thickness. If multiple layers are considered, only the layers of similar geology should be lumped together as the ERST is simplified to consider only the dominant protective layer. The groundwater section of the ERST is only addressing the risk to the UGR below the site and not contemplating lateral movement of potential manure constituents.
- Predominant geology of the PL Using the most specific site information; indicate the geology of the protective layer. If the material is very heterogeneous (i.e. multiple layers of different geologic materials), then the dominant geologic unit that has the lowest hydraulic conductivity should be considered.
- Estimated subsoil texture of the PL Subsoil texture refers to the predominant grain size distribution. Using the "Estimating Subsoil Texture" table in Appendix 4, information about the geology of the PL can be used to estimate the subsoil texture (i.e. fine, medium, coarse or very coarse). For example, a clay PL would be assigned a "fine" subsoil texture using the table. For reference, a hydraulic conductivity scale is also included in the table to allow for estimating of hydraulic conductivity. If the material is a glacial till with high clay content, choose a subsoil texture that is finer in the range. If the glacial till is sendier, then choose a subsoil texture that is coarser in the range. If the glacial till is coarser in the range. If a layer of clay or glacial till contains amounts of silt, sand or gravel that are likely to be dominant for transport of groundwater, then the appropriate range for that material should be used. At a facility where a liner has been constructed, use the native subsoil under the facility when determining the subsoil texture of the protective layer.
- PL measured From (e.g. surface, at specific depth) and To the chosen protective layer is not always a geologic unit found at the surface. Indicate what depth the unit starts 'From' and ends 'To'. There may be multiple layers that are used – indicate these separately in additional notes. If multiple layers are considered as one unit, enter the top of the unit as 'From' and the bottom of the unit as 'To'.

10. Infiltration Potential and Surface Water Runoff

 Average annual precipitation – Estimate the annual total precipitation using the "Annual Total Precipitation of Alberta, 1971 to 2000" (Alberta Agriculture) map in Appendix 4. Appendix B

Site Borehole Logs and Locations

advanced August 9, 2019

CHILAKO DRILLING SERVICES LTD

Box 942 Coaldale, Alberta, T1M 1M8 (403) 345-3710

SOIL PROFILE AND PARENT MATERIAL DESCRIPTION

Site Location: Arie Muilwijk

Date: 09-Aug-19

Hole #	Location	Depth	Texture	Moisture	Geological	Sample	Remarks
AM1-19	0314346	0-2.1	VFSL	SM	Lac		Silty
	5511364	2.1-3.5	VFSCL	VM	Lac		
		3.5-5.1	VFSL	VM-Sat	Lac		
		5.1-5.9	SiCL	Μ	Lac		V. firm, med-high plastic, yellow brown
		5.9-6.2	FSCL	VM	Lac		Slough @ 3.3m
AM2-19	0314354	0-2.9	VFSL	SM	Lac		Silty
	5511400	2.9-3.6	SiCL	VM	Lac		Sandy
		3.6-5.6	VFSL	Sat	Lac		Soft, olive brown, silty, free water
		5.6-6.2	SiCL	М	Lac		V. firm, med-high plastic, olive brown
							slough @ 3.9m
AM3-19	0314364	0-1.8	VFSL	м	Lac		Loose, olive brown, silty
	5511294	1.8-2.3	VFSCL	VM	Lac		Low plastic, olive brown, silty
		2.3-3.0	VFSL	VM	Lac		Silty
		3.0-4.1	VFSL	Sat	Lac		Silty, free water, VFSL sand lenses
		4.1-4.6	SiCL	М	Lac		Stiff, med plastic, olive brown
		4.6-5.0	VFSCL	VM	Lac		Soft, low plastic, olive brown
		5.0-6.2	SiCL	VM	Lac		Firm, low plastic, olive brown
AM4-19	0314411	0-1.0	SiCL	М	Lac		
	5511281	1.0-2.7	VFSL	M	Lac		
		2.7-4.4	VFSL	Sat	Lac		Soft
		4.4-6.2	C-SC	Μ	Till		Stiff, low plastic, trace gravel

Legend: L

L Loam C Clay S Sand Gr. Gravel Si Silt F Fine (sand) VF Very Fine (sand)

Eg. VFSCL = Very Fine Sandy Clay Loam



AO: Calculations made to try to replicate the hydraulic conductivity calculations made in the Wood Environment and Infrastructure Solutions report.

Andy Cumming NRCB Approval Officer Lethbridge, AB andy.cumming@nrcb.ca

RE: Arie Muilwijk NE 10-9-27 W4

November 26, 2020

Hi Andy,

Thank you for accepting my offer on November 23, 2020 to provide you with a written analysis of the average calculated permeability on page 4 of the Compliance Report – Roller Compacted Concrete for Calf Shelter, Calf/Feeder Pens (dated November 6, 2020), from Wood Environment and Infrastructure Solutions ("Wood").

Wood information

Wood stated"the average calculated permeability through the 150mm thick RCC mat would be 9.0x10⁻⁸ cm/sec."

Wood provided:

- Overall area of RCC mat of 10m by 10m
- A 20mm wide crack in both directions in the overall area
- RCC permeability is 1x10⁻⁹ cm/sec
- Crack permeability is 1x10⁻⁴ cm/sec

Wood did not provide the methodology used or the calculations that arrived at their stated average calculated permeability.

<u>Analysis</u>

An applicable methodology that uses area and permeability is Darcy's Law:

Q = kiA

(Equation 1)¹

where Q is the flow rate k is the hydraulic conductivity/permeability i is the hydraulic gradient A is the area

As the information provided by Wood are inputs into Equation 1, I will use Darcy's Law methodology and provide my calculations in an attempt to duplicate the Wood result for average calculated permeability of 9.0×10^{-8} cm/sec. In this report, I will refer to this value as the overall permeability (k_o).

¹ Groundwater, Freeze and Cherry, Page 16.

I assumed that the flow rate through the overall area (Q_0) will be equal to the sum of the flow rate through the area of the cracks (Q_c) and the flow rate through the uncracked area (Q_U) . In equation form, this assumption reads:

$$Q_0 = Q_C + Q_U$$
 (Equation 2)

Expanding equation 2 by substituting equation 1 for each Q provides:

$$k_{oio}A_{o} = k_{cic}A_{c} + k_{uiu}A_{u}$$
 (Equation 3)

Darcy's Law is valid for analysis of liners for solid manure. However, making a reasonable numeric assumption of a hydraulic gradient (i) for solid manure is difficult because it requires information (or assumptions) about hydraulic head. Instead, I make the assumption that the hydraulic gradient (i) will be the same for the flow rate in the overall area, the cracked area, and the uncracked area:

$$i_0 = i_c = i_U$$
 (Equation 4)

Substituting equation 4 into equation 3 (all hydraulic gradients would then be i_0), then dividing both sides of equation 3 by i_0 yields:

$$k_0A_0 = k_cA_c + k_0A_0$$
 (Equation 5)

Table 1 lists the data provided by Wood, and the assigned variables and resulting calculations (if any). All of the variables in Equation 5 have a numeric value listed in Table 1, except the variable I am trying to determine (k_0).

Table 1. Assigned variables and calculations

Wood data	Variable and	Calculation (if any)					
	Abbreviation	••••••••••••••••••••••••••••••••••••••					
	ADDIEVIALION						
Overall area of RCC mat of 10m by 10m	Area overall (A ₀)	10m x 10m= 100m ²					
Two cracks 20mm wide in overall area	Area of cracks (A _c)	20mm=0.02m x 2 x 10m					
		= 0.4m ²					
	Uncracked area (A _∪)	$A_U = A_O - A_C = 100 - 0.4 =$					
		99.6m ²					
RCC permeability is 1x10 ⁻⁹ cm/sec	Permeability of						
	uncracked RCC (k _∪)						
Crack permeability is 1x10 ⁻⁴ cm/sec	Permeability of cracks						
	(k _c)						

Dividing both sides of equation 5 by A_O yields

 $k_{O} = [k_{C}A_{C} + k_{U}A_{U}]/A_{O} \qquad (Equation 6)$

Substituting numeric values from Table 1 into Equation 6 and solving

$$k_{0} = [(1x10^{-4} \text{ cm/sec } x \ 0.4\text{m}^{2}) + (1x10^{-9} \text{ cm/sec } x \ 99.6\text{m}^{2})] / 100\text{m}^{2}$$

$$k_{0} = [4x10^{-5} \text{ m}^{2} \text{ cm/sec} + 9.96x10^{-8} \text{ m}^{2} \text{ cm/sec}] / 100\text{m}^{2}$$

$$k_{0} = [4.00996x10^{-5} \text{ m}^{2} \text{ cm/sec}] / 100\text{m}^{2}$$

$$k_{0} = 4.00996x10^{-7} \text{ cm/sec}$$

My analysis indicates that the overall permeability (k_0) for RCC using Darcy's Law is $4x10^{-7}$ cm/sec ($40x10^{-8}$ cm/sec).

Using the methodology and assumptions listed above, I was not able to duplicate the Wood result for average calculated permeability/overall permeability of 9.0x10⁻⁸ cm/sec.

In closing, please contact me if you have any questions.

Scott Cunningham Scott Cunningham, P.Eng., P.Ag.

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